

Multiple DC Solution Determination using VHDL-AMS

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Problem and Proposed Approach

The investigation of nonlinear resistive networks is one of the fundamental tasks in circuit simulation. Relative difficult problems that have to be solved are:

- Finding the multiple DC solutions of circuits as flip-flops, Schmitt-triggers, and negative resistance circuits.
- Calculation of multivalued transfer characteristics of nonlinear resistive networks (e.g. of Schmitt-triggers).
- Calculation of the turning points of multivalued transfer characteristics (e.g. in order to determine hysteresis or pull-in voltages in electromechanical systems).

Continuation techniques based on homotopy methods are typically applied to solve these problems whereas these methods are implemented in customized simulators.

Proposed way in the presented paper:

- Direct application of the homotopy idea to the network analysis problem by creating a modified and augmented network that is similar to the original one.
- Constitutive relation of the modified subnets can be expressed using a behavioral description language, e. g. VHDL-AMS.
- Solution of the modified network using an available VHDL-AMS simulation engine. From the solution of the modified and augmented network we get the solution we are interested in.

An advantage of the suggested approach is that no special simulation engine is necessary. All features of available VHDL-AMS simulation engines can be used.

Homotopy Methods

- For the analysis of nonlinear resistive networks a system of nonlinear equations has to be solved: $F(x) = 0$, where $F: \mathbb{R}^n \rightarrow \mathbb{R}^n$
- Continuation methods based on a homotopy function $H: \mathbb{R}^n \times \mathbb{R} \rightarrow \mathbb{R}^n$ with the following characteristics:
 - The solution $x_0 \in \mathbb{R}^n$ of $H(x_0, \lambda_0) = 0$ can be determined for a given $\lambda_0 \in \mathbb{R}$.
 - For a special $\lambda_f \in \mathbb{R}$ the solution $x_f \in \mathbb{R}^n$ of $H(x_f, \lambda_f) = 0$ is also a solution of F , i. e. $F(x_f) = 0$.
- The solution is calculated by following the solution curve $L = \{ (x, \lambda) \in \mathbb{R}^n \times \mathbb{R} \mid H(x, \lambda) = 0 \}$ from (x_0, λ_0) to (x_f, λ_f) .
- L can be traced for instance by solving the following DAE

$$\begin{aligned} H(x, \lambda) &= 0 \\ \sum_{i \in I} x_i'(t)^2 + \lambda'(t)^2 &= 1, \quad \text{where } (x(0), \lambda(0)) = (x_0, \lambda_0). \end{aligned}$$

I is a set of essential variables for curve tracing. t is a pseudo arc length of the solution curve L .

Network Formulation

- Assume a resistive network N is given. We construct a modified network N_λ that is close-by the original. λ is an additional quantity. N is in accordance with F . N_λ corresponds to the homotopy function H .
- To calculate the DC operating point, the modification can be done for instance by
 - Replacement of independent voltage and current sources with values V_{cl} and I_{cl} resp. by sources with values $\lambda \cdot V_{cl}$ and $\lambda \cdot I_{cl}$ (*source stepping*).
 - Replacement of open branches by additional current sources with values $(1-\lambda) \cdot I_{c0}$ (*artificial input current source stepping*).
 - ... *G-min stepping*, ...

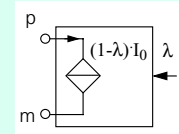
Operating points can be detected in these cases for $\lambda=1$.
- N_λ is augmented by a subsystem that realizes the equation $\sum_{i \in I} p_i x_i'(t)^2 + \lambda'(t)^2 = 0$. The output λ of this subsystem drives the modified sources and conductances.
- The augmented network can be evaluated with the time domain simulation algorithm of the simulation engine. The condition $\lambda=1$ can be detected using the 'ABOVE attribute of VHDL-AMS.
- Determination of transfer characteristics and turning points can be done in an equivalent manner.

Network Modifications (N_λ)

```
entity css is
  generic (vc0 : real := 0.0);
  port (terminal p, m : electrical;
        quantity lambda : in real);
end entity css;

architecture a0 of css is
  signal i0 : real;
  quantity v across i through p to m;
begin
  process(domain) is begin
    i0 <= i;
  end process;

  if domain = quiescent_domain use
    v == vc0;
  else
    i == (1.0-lambda)*i0;
  end use;
end architecture a0;
```



Artificial input current source

```
entity trace is
  generic (N : natural := 1;
          ta : real := 1.0e-3;
          tb : real := 5.0e-3);
  port (quantity x : in real_vector (1 to N);
        quantity lambda : out real);
end entity trace;

architecture a1 of trace is
  quantity lambda_dot : real;
  quantity x_help, x_dot : real_vector (1 to N);
  function factor (t: real; ta : real; tb : real)
    return real is
    variable th : real;
  begin
    th := (t-ta)/(tb-ta);
    return (3.0*th*th - 2.0*th*th*th);
  end function factor;
begin
  lambda_dot == lambda_dot;
  x_help == x;
  x_dot == x_help;
  if now < ta use
    lambda == now;
  elsif now < tb use
    lambda_dot == lambda_dot*lambda_dot
      + factor(now,ta,tb)*(x_dot*x_dot);
  else
    lambda_dot == lambda_dot*lambda_dot + x_dot*x_dot;
  end use;
end architecture a1;
```

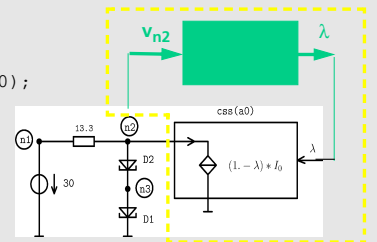
$$\sum_{i \in I} x_i'(t)^2 + \lambda'(t)^2 = 1$$

Model realizes

Multiple DC Solutions (Two-Tunnel-Diode Circuit)

```
entity detect is
  port (quantity lambda : in real;
        terminal p_voltage : electrical;
        signal s_voltage : out real := 0.0);
end entity detect;

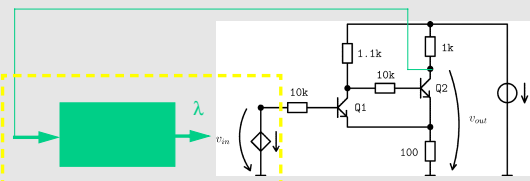
architecture one of detect is
  quantity v across p_voltage;
begin
  process (lambda'above(1.0)) is
  begin
    s_voltage <= v;
  end process;
end architecture one;
```



Modified and augmented network

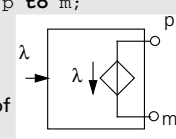
Subcircuit to detect $\lambda = 1$ (driven by λ , observes voltage at p_voltage)

Calculation of Multivalued Transfer Characteristics (Schmitt-Trigger)

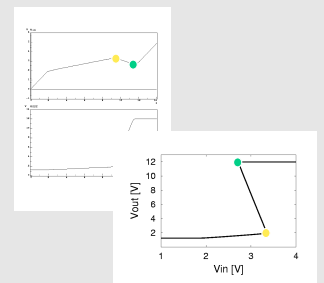


```
entity vss is
  port (terminal p, m : electrical;
        quantity lambda : in real);
end entity vss;

architecture a0 of vss is
  quantity v across i through p to m;
begin
  v == lambda;
end architecture a0;
```



Input voltage source for calculation of multivalued transfer characteristics

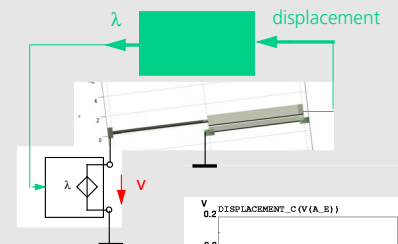


Result of transient simulation and transfer characteristic $v_{out}(v_{in})$

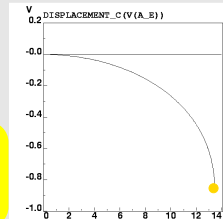
Determination of Turning Points (Pull-in Voltage Calculation)

```
entity detect is
  port (terminal p_voltage : electrical;
        signal s_voltage : out real := 0.0;
        signal stop : out boolean);
end entity detect;

architecture turning of detect is
  quantity v across p_voltage;
begin
  process is
  begin
    stop <= false;
    wait on domain;
    while true loop
      wait on v'dot'above(0.0);
      s_voltage <= v;
      stop <= true;
    end loop;
  end process;
end architecture turning;
```



Transfer characteristic: Displacement as function of v; Turning point delivers the pull-in voltage



Subcircuit to detect the turning point