



# A high-level VHDL-AMS model design methodology for analog RF LNA and Mixer

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# Outline

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- Introduction
- Design Approach
- Model Validation In The Case of LNA
- Conclusion



# Introduction

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- Mixed signal System On Chip
  - Rapidly increasing transistors density
  - The booming market of wireless applications
- Gap between
  - need of rapid time-to-market
  - complex design and verification procedure of the SOC's
- Need for SoC model library
  - A need exists to create a SoC model library include RF models
  - Support Top down design for the SoCs.



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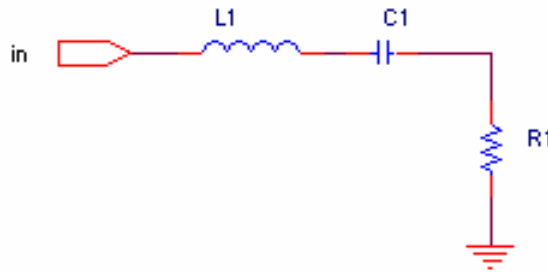
# Design Approach

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- Modeling the impedance matching
- Modeling the function of the RF block
- Modeling the bandwidth
- Modeling the noise
- Modeling the non-linearity
- Design flow

# Modeling the impedance matching

- LRC network is chosen to be the basic frame.



$$\omega_0 = \frac{1}{\sqrt{LC}}$$

- R1 equals to  $50\Omega$  matching with the input  $50\Omega$  source impedance.
- L1 and C1 are resonant at designed frequency  $\omega_0$ .
- The value of L1 is set to an experienced value according to the designed frequency  $\omega_0$ .



# Modeling the function of RF block

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- LNA

- Function:

- Gain

- Model expression:

- The input signal is multiplied by a constant

- MIXER

- Function:

- Provide frequency translation and/or gain.

- Model expression:

$$(A\cos\omega_1 t)(B\cos\omega_2 t) = \frac{AB}{2} [\cos(\omega_1 - \omega_2)t] [\cos(\omega_1 + \omega_2)t] \text{---(1)}$$



# Modeling the bandwidth

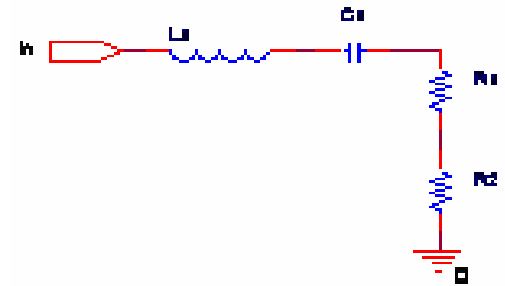
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- Behavioral model of filter in VHDL-AMS
  - Restriction to model a user-specified filter in VHDL-AMS.
    - VHDL-AMS supports Laplace transforms by providing the predefined 'LTF attribute of a quantity.
    - The 'LTF attribute requires both numerator and denominator coefficient lists that are required to be static expressions.
  - Overcome this difficulty.
    - Exploited a filter model generator to produce models from dynamic model parameters [7].
- Butterworth bandpass filter is chosen to model the bandwidth of RF components.
  - Use 0.2dB instead of 3dB as the attenuation limit.



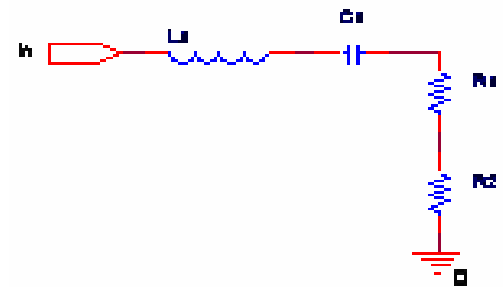
# Modeling the noise

- Noise Figure
  - A very important specification of LNA and Mixer.
  - Is chosen to be the one of the specifications of the model.
- Solution
  - Two parallel connected resistors are used instead of one resistor in the input RLC network.



# Modeling the noise

- Solution (continued)
  - R1 is a noisy resistor.
  - R2 is a ideal/non-noisy resistor.
  - The value of R1 is initialized to be 25ohm.
  - According to the specified noise figure, the design tool optimized the value of R1 by bisection algorithm.
  - To keep the model's input impedance matching at the designed frequency, R2 equals 50 minus the value of R1.





# Modeling the non-linearity

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- IIP3

- A very important characteristic of LNA and Mixer.
- Is chosen to be the one of the specifications of the model.

- Solution

- Assume the non-linear behavior of the RF circuit

is 
$$y(t) \approx \alpha_1 x(t) + \alpha_2 x(t)^2 + \alpha_3 x(t)^3 \text{ --- (2)}$$

when  $x(t)$  are the input signals with different frequency and assume

$$x(t) = A_1 \cos \omega_1 t + A_2 \cos \omega_2 t \text{ --- (3)}$$



# Modeling the non-linearity

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- Solution(continued)

- $Y(t)$  has the following intermodulation products[6]:

$$\omega = \omega_1 \pm \omega_2 : \alpha_2 A_1 A_2 \cos(\omega_1 + \omega_2)t + \alpha_2 A_1 A_2 \cos(\omega_1 - \omega_2)t$$

$$= 2\omega_1 \pm \omega_2 : \frac{3\alpha_3 A_1^2 A_2}{4} \cos(2\omega_1 + \omega_2)t + \frac{3\alpha_3 A_1^2 A_2}{4} \cos(2\omega_1 - \omega_2)t$$

$$= 2\omega_2 \pm \omega_1 : \frac{3\alpha_3 A_2^2 A_1}{4} \cos(2\omega_2 + \omega_1)t + \frac{3\alpha_3 A_2^2 A_1}{4} \cos(2\omega_2 - \omega_1)t$$

and fundamental components[6]:

$$\omega = \omega_1 : \left( \alpha_1 A_1 + \frac{3}{4} \alpha_3 A_1^3 + \frac{3}{2} \alpha_3 A_1 A_2^2 \right) \cos \omega_1 t$$

$$\omega_2 : \left( \alpha_1 A_2 + \frac{3}{4} \alpha_3 A_2^3 + \frac{3}{2} \alpha_3 A_2 A_1^2 \right) \cos \omega_2 t$$



# Modeling the non-linearity

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- Solution(continued)
  - Since other frequency in inter-modulation products of the two tone signal are not big concern, the equation (2) is enough to model non-linearity.

$$y(t) \approx \alpha_1 x(t) + \alpha_2 x(t)^2 + \alpha_3 x(t)^3 \text{ ---- (2)}$$

- IMD (IM Distortion)[6]:

The ratio of the amplitude of the output third-order products to  $\alpha_1 A$ .
- Compute IIP3[6]:

$$IIP_3 |_{dBm} = \frac{IMD}{2} + P_{in} |_{dBm}$$



# Modeling the non-linearity

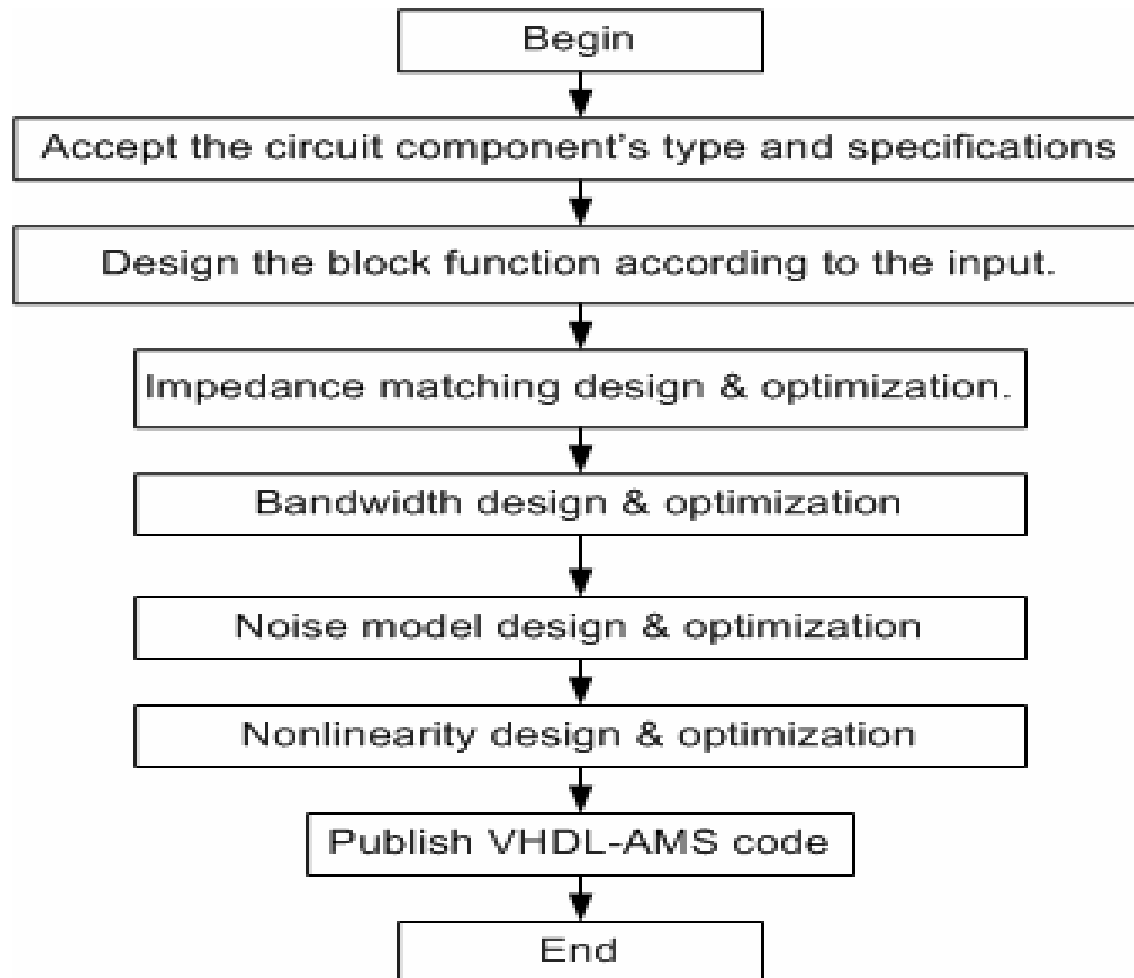
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- Solution (continued)
  - Parameters optimization
    - $\alpha_1$  is set to be 1 to fulfill the gain specification.
    - For  $\alpha_2$ , Since the intermodulation product of  $\omega_1 \pm \omega_2$  is not the concern,  $\alpha_2$  is set to be 1.
    - For  $\alpha_3$ , according to the specified IIP3, the design tool optimized the value of  $\alpha_3$  by bisection algorithm.

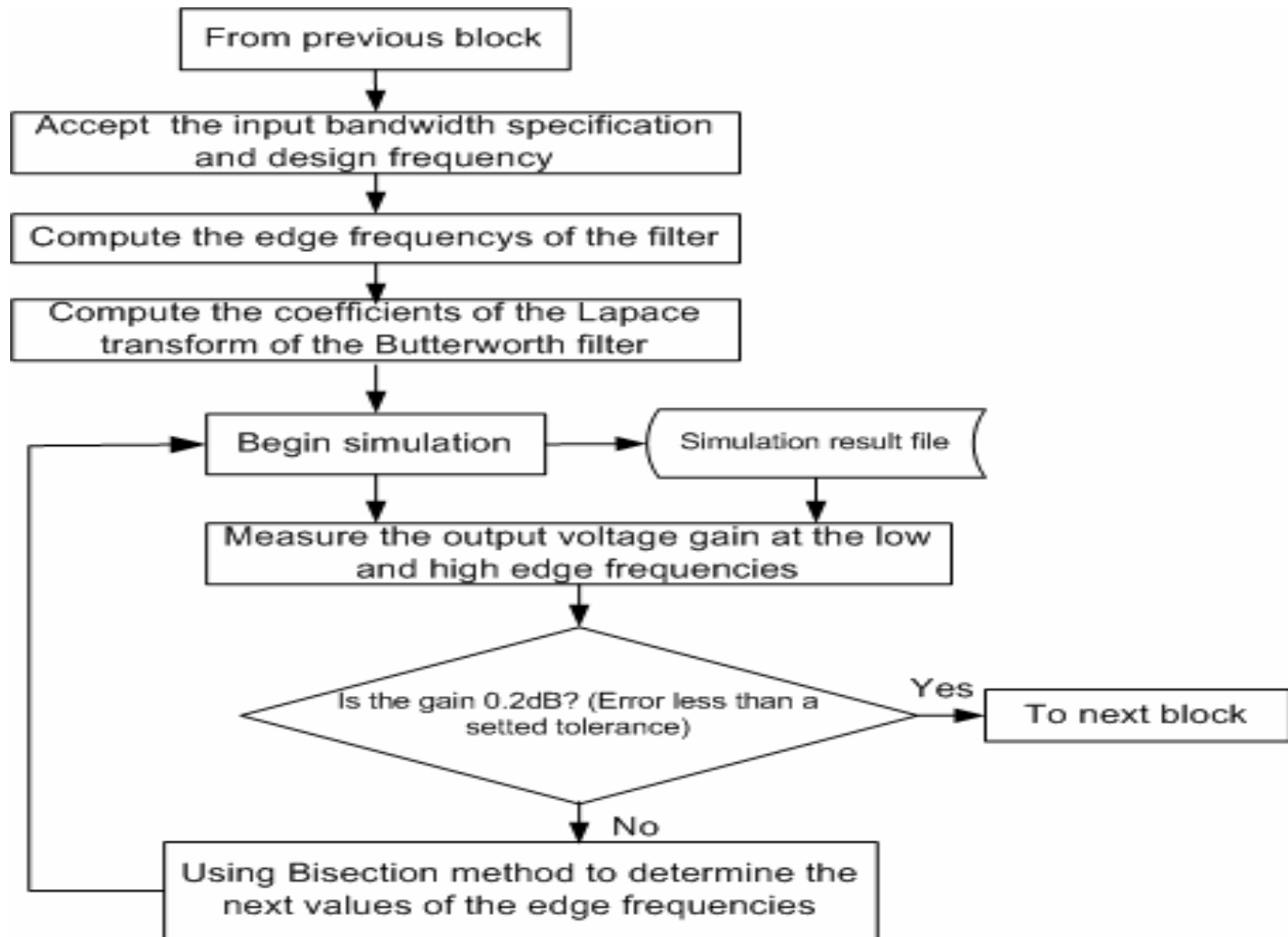


# Design Flow

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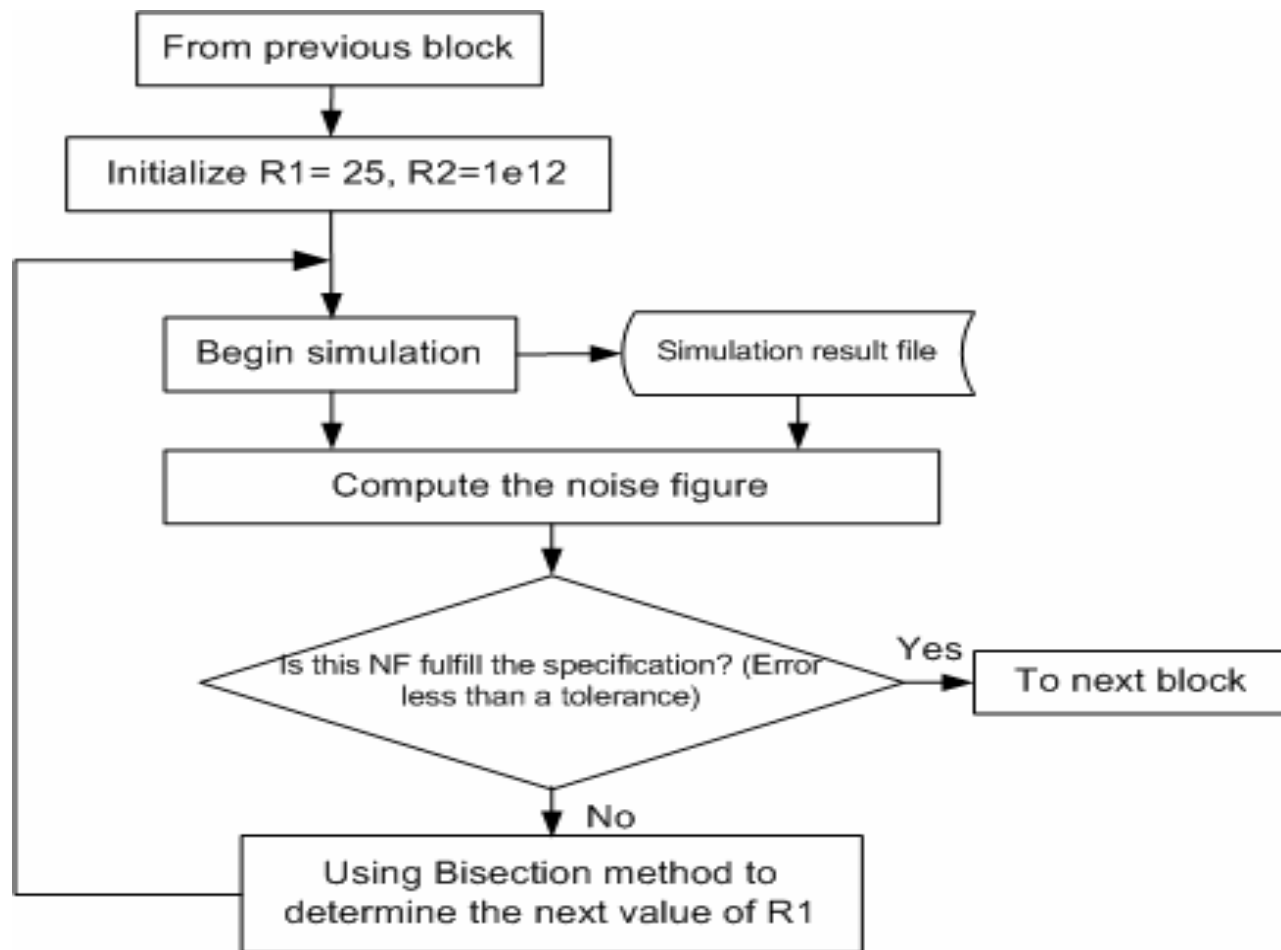


# Design Flow of the bandwidth modeling





# Design Flow of the noise modeling





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# Model Validation of LNA

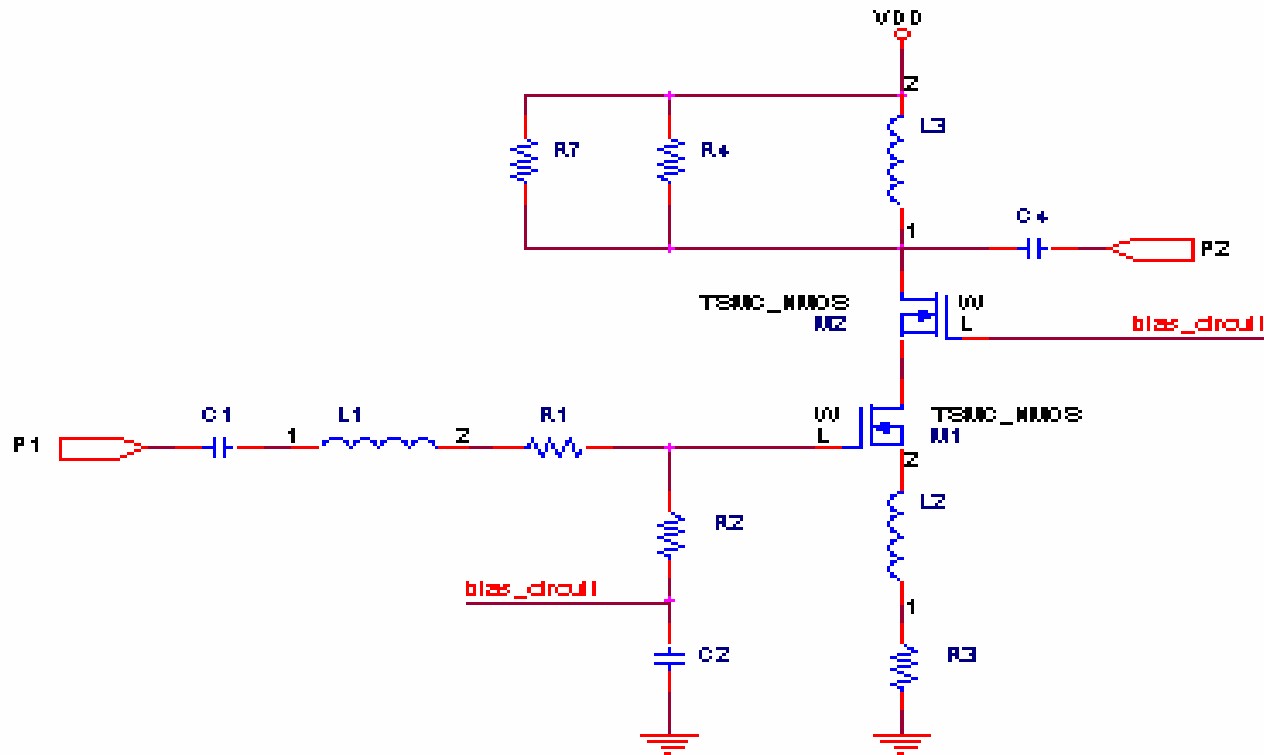
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- Design Specifications

Gain	17.1dB
Bandwidth	>25M
Noise Figure	0.775dB
IIP3	3.6dBm

# Model Validation of LNA

- Transistor-level 1.9GHz LNA in TSMC25 technology





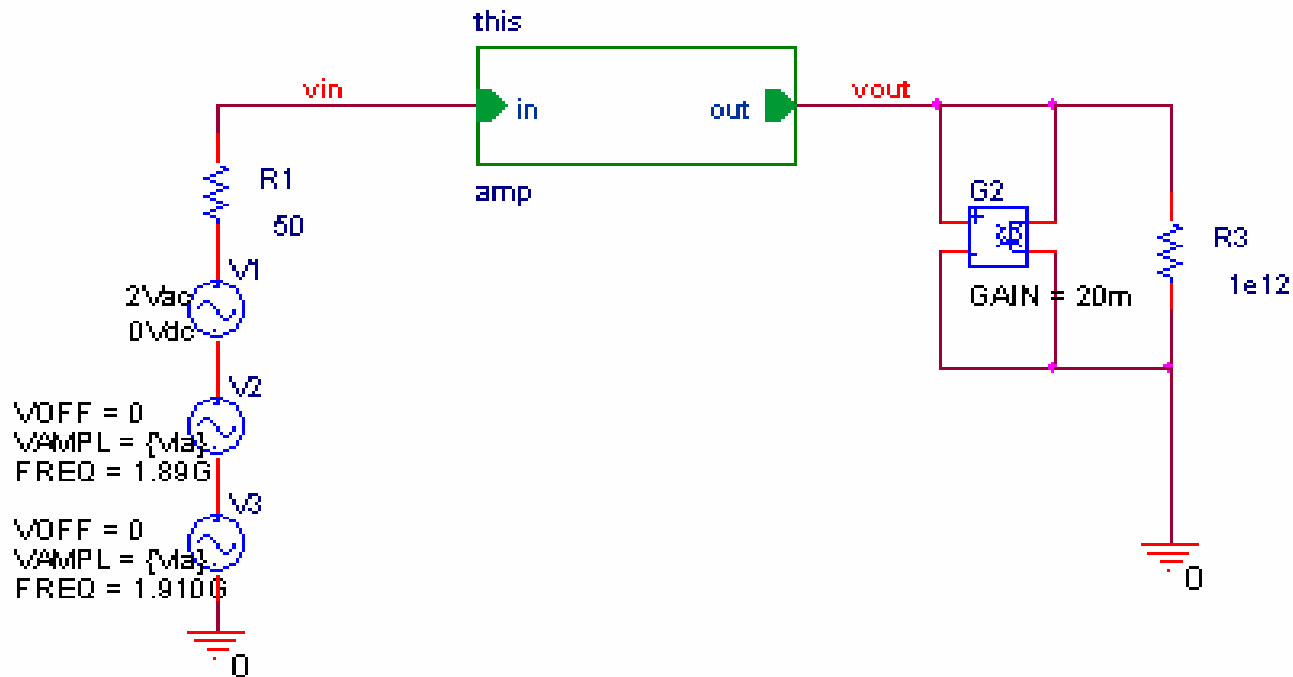
# Model Validation of LNA

- Parameters in the behavioral LNA model

L1	10nH
C1	701.67fF
R1	9.75ohm
R2	40.25ohm
Laplace transfer function	$\frac{3769911040.0s}{142517087507302055936.0 + 3769911040.0s + s^2}$
Coefficients for the non-linearity expression	$\alpha_1 = 1, \alpha_2 = 1, \alpha_3 = 0.1183$

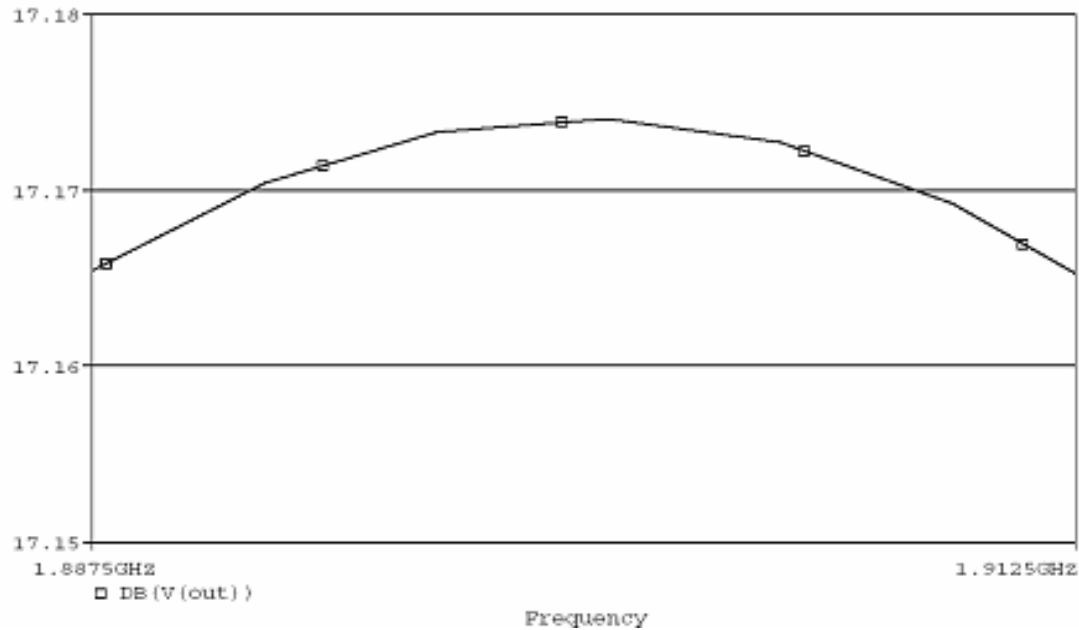
# Model Validation of LNA

- Test circuit of LNA



# Model Validation of LNA

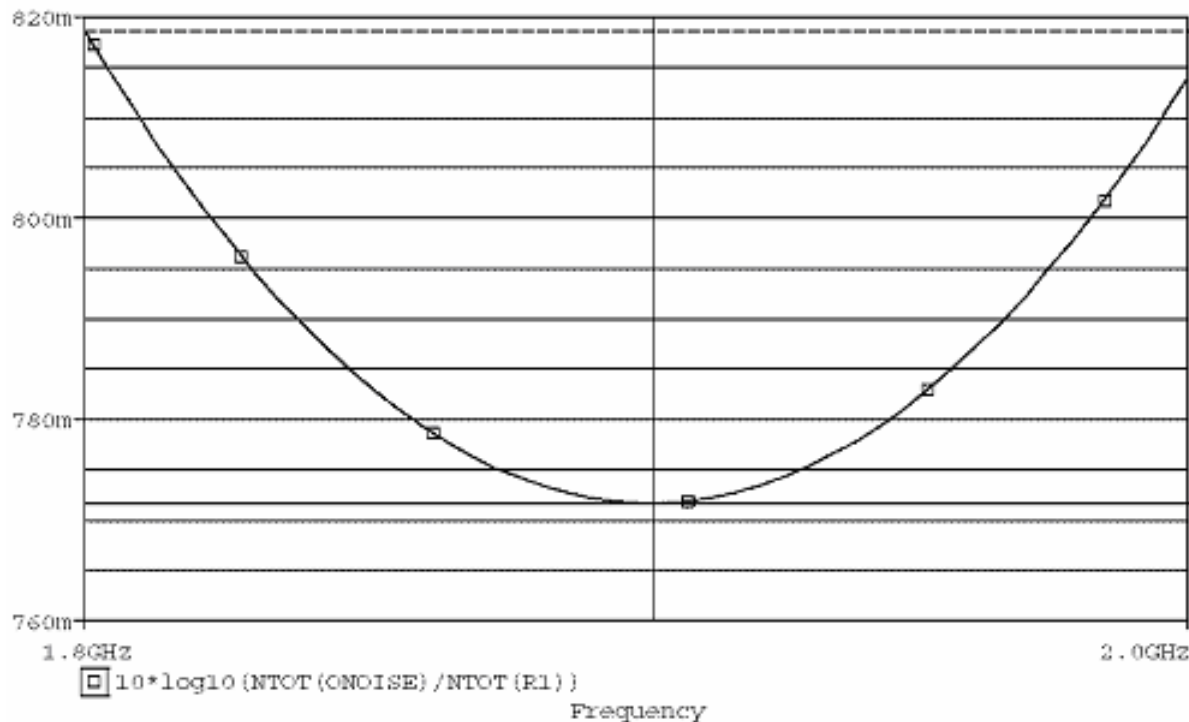
- Gain and Bandwidth Simulation for behavioral LNA model



- The gain variation between 1.8875Ghz and 1.9125Ghz is 0.01db, the bandwidth requirement is met.

# Model Validation of LNA

- Noise Figure Simulation for behavioral LNA model

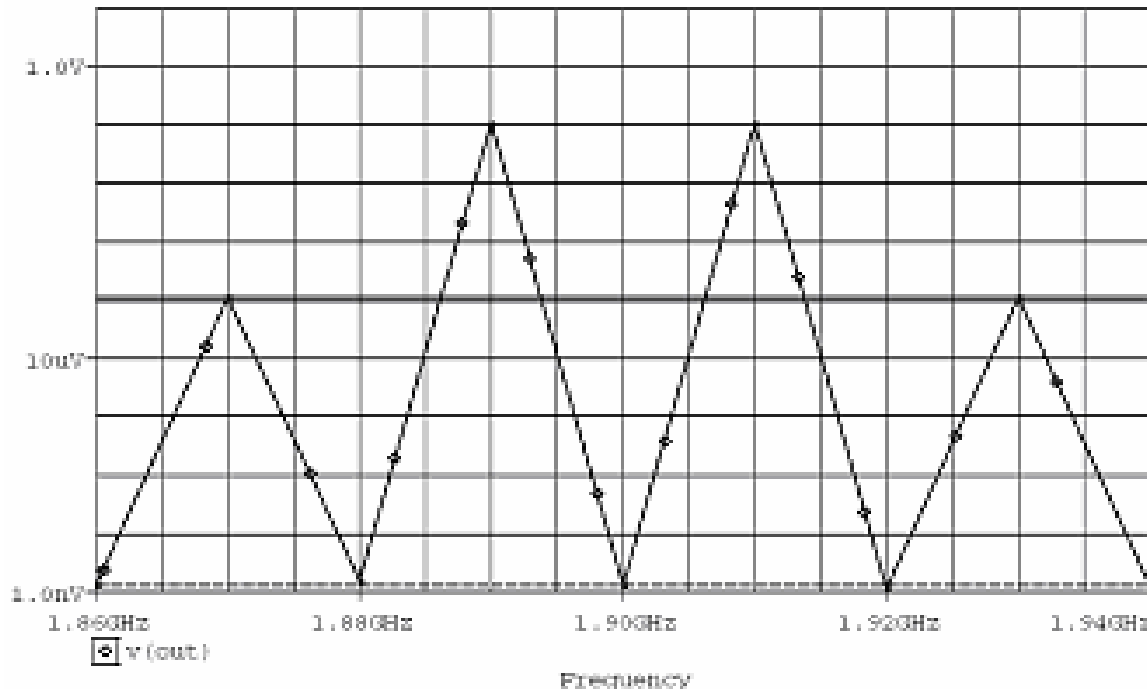


- the noise figure at 1.9Ghz is 0.772dB.



# Model Validation of LNA

- Two-tone analysis for behavioral LNA model



- IIP3 equals to 3.52dBm



# Model Validation of LNA

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- Comparison between the design specification and the simulation result of the behavioral model.

	Design specification	Simulation result of behavioral model
Gain	17.1dB	17.174dB
Bandwidth	>25M	>25M
Noise figure	0.775dB	0.772dB
IIP3	3.6dBm	3.52dBm



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# Conclusion

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- The methodology is not necessarily general for all RF components, but is applicable to LNA and MIXER.
- In the future, this methodology will be extended to design oscillators and PLLs.
- To support RF circuit and system simulation and verification, harmonic analysis or FFT function and noise simulation must be supported by the VHDL-AMS simulator.



# Reference

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Thank you.

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Questions and Answers.