Verification of an Automotive Application Using Smart Component Headlight Leveling Circuit and Property Extraction

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Never stop thinking

Overview



Introduction to Headlight Leveling

- Application Description
- Application Modeling
- Smart Component Extraction

Comparing Component measurements with simulation results

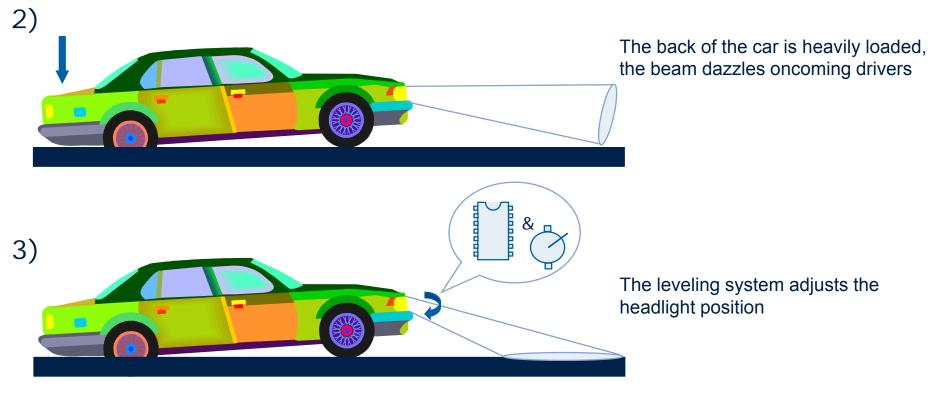
Application Verification (simulation)

Introduction to Headlight Leveling



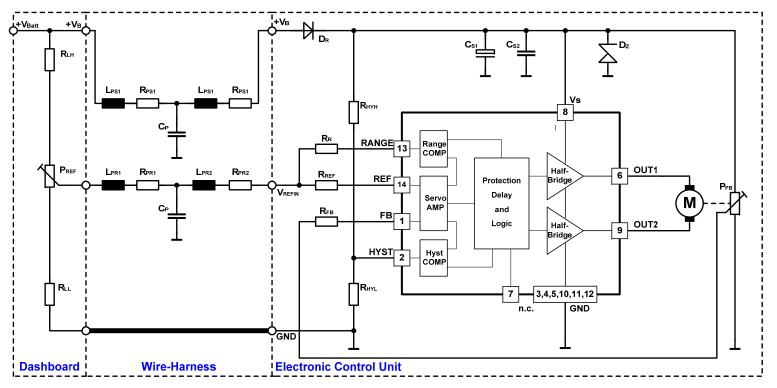


In normal load condition, the beam lights the road ahead





Application Description



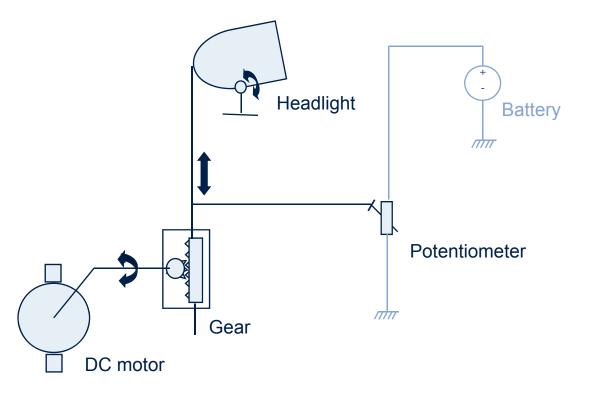
The headlights are moved by a DC motor, which is controlled by a fullbridge circuit (H-Bridge)

One reference value is set (Pref) and compared to a feedback value (PFb) by the logic part of the circuit

Application Description (2)



- The Mechanical Part of the system contains:
 - DC Motor
 - □ Gear
 - Headlight
 - Potentiometer



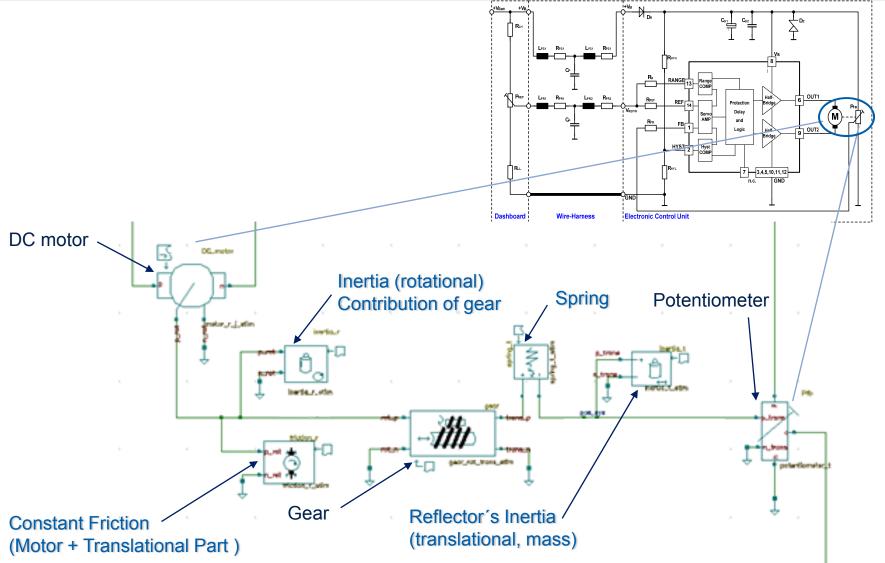
Application Modeling



- The Electronical Components (except the circuit) and the Mechanical Part are modelled using VHDL-AMS
- The circuit is integrated on transistor-level
- The models ´ equations are based on electro / mechanical conservation laws
- The models of the Mechanical Part contains following blocks:
 - DC Motor
 - □ Gear
 - Potentiometer
 - + friction and inertia, considered as separated contributors

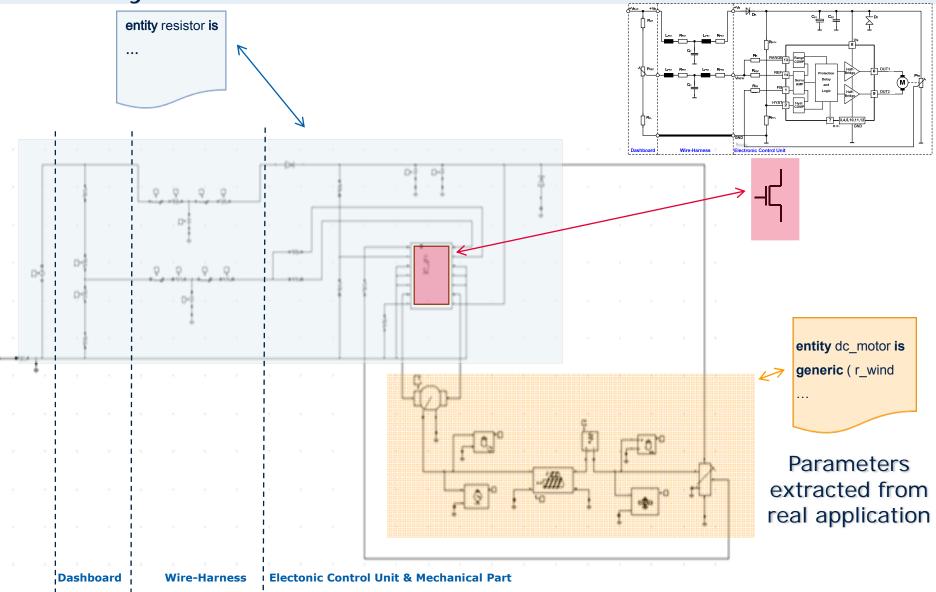
Application Modeling (2) Mechanical Part





Application Modeling (3) Whole system





Smart Component Extraction



- All parameters are extracted from simple measurements performed on the real application
- Parameters are listed here:

Part	Parameters
DC motor	Armature resistance R
	Armature inductance L
	Torque constant Kr
	Back-emf constant Ke
	Damping D
	Moment of Inertia J
Constant friction	Friction Test,
	Tcst = Tcst_motor + Tcst_system
Gear inertia	Moment of Inertia Jg
Gear	Gear ratio gear_ratio
	Pinion radius radius_p
Spring	Spring constant Ks
Reflector	Reflector's mass extrapolated to the output of the gear mass extrapolated
Potentiometer	Factor k
rotentiometer	Pactor k

DC motor parameters extraction is hightlighted in what follows

Smart Component Extraction (2) DC Motor equations



 $T = -Kt * i + D * \omega + J * d(\omega)/dt$

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Smart Component Extraction (3) DC Motor equations



 $T = -Kt * i + D * \omega + J * d(\omega)/dt$ - generated torque (Kt : torque coefficient)

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Smart Component Extraction (4) DC Motor equations



 $T = -Kt * i + D * \omega + J * d(\omega)/dt$ - generated torque (Kt : torque coefficient)

- viscous damping loss (D : damping coefficient)

Smart Component Extraction (5) DC Motor equations



 $T = -Kt * i + D * \omega + J * d(\omega)/dt$

- generated torque (Kt : torque coefficient)
- viscous damping loss (D : damping coefficient)
 - inertial losses (J : moment of inertia)

Smart Component Extraction (6) DC Motor equations



$T = -Kt * i + D * \omega + J * d(\omega)/dt$

- generated torque (Kt : torque coefficient)
- viscous damping loss (D : damping coefficient)
- inertial losses (J: moment of inertia)

$U = Ke * \omega + R * i + L * d(i)/dt$

Smart Component Extraction (7) DC Motor equations



$T = -Kt * i + D * \omega + J * d(\omega)/dt$

- generated torque (Kt : torque coefficient)
- viscous damping loss (D : damping coefficient)
- inertial losses (J: moment of inertia)

```
U = Ke * ω + R * i + L * d(i)/dt
- back-EMF (Ke : EMF coefficient)
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Smart Component Extraction (8) DC Motor equations



$T = -Kt * i + D * \omega + J * d(\omega)/dt$

- generated torque (Kt : torque coefficient)
- viscous damping loss (D : damping coefficient)
- inertial losses (J: moment of inertia)

$U = Ke * \omega + R * i + L * d(i)/dt$ - back-EMF (Ke : EMF coefficient)

- winding resistance voltage drop (R : winding resistance)

Smart Component Extraction (9) DC Motor equations



$T = -Kt * i + D * \omega + J * d(\omega)/dt$

- generated torque (Kt : torque coefficient)
- viscous damping loss (D : damping coefficient)
- inertial losses (J: moment of inertia)

$U = Ke * \omega + R * i + L * d(i)/dt$

- back-EMF (Ke : EMF coefficient)
- winding resistance voltage drop (R: winding resistance)
 - winding inductance voltage drop (L : winding inductance)

Smart Component Extraction (10) DC Motor equations



$T = -Kt * i + D * \omega + J * d(\omega)/dt$

- generated torque (Kt : torque coefficient)
- viscous damping loss (D : damping coefficient)
- inertial losses (J: moment of inertia)

Note: Kt = Ke when SI units are used

$U = Ke * \omega + R * i + L * d(i)/dt$

- back-EMF (Ke : EMF coefficient)
- winding resistance voltage drop (R: winding resistance)
- winding inductance voltage drop (L: winding inductance)

Smart Component Extraction (11) DC Motor equations



$T = -Kt * i + D * \omega + J * d(\omega)/dt$

- generated torque (Kt : torque coefficient)
- viscous damping loss (D : damping coefficient)
- inertial losses (J: moment of inertia)

$U = Kt * \omega + R * i + L * d(i)/dt$

- back-EMF (Ke = Kt)

- winding resistance voltage drop (R: winding resistance)

- winding inductance voltage drop (L: winding inductance)

Smart Component Extraction (12) DC Motor Parameter extraction



- L extraction :

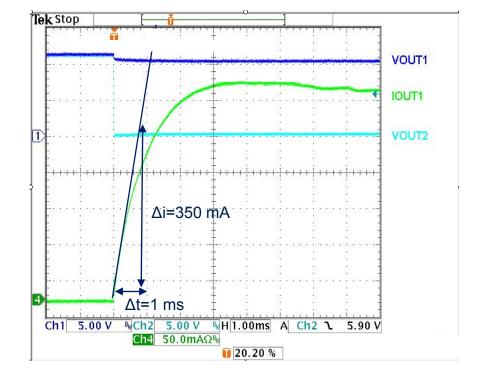
 $U = Kt * \omega + R * i + \mathbf{L} * d(i)/dt$

• Motor in inrush

• U =
$$\underbrace{Kt * \omega}_{=0} + \underbrace{R * i}_{=0} + L * d(i)/dt$$

• the slope is measured:

 $\mathbf{L} = \mathbf{U} * \Delta t / \Delta i$



Smart Component Extraction (13) DC Motor Parameter extraction



- R extraction :

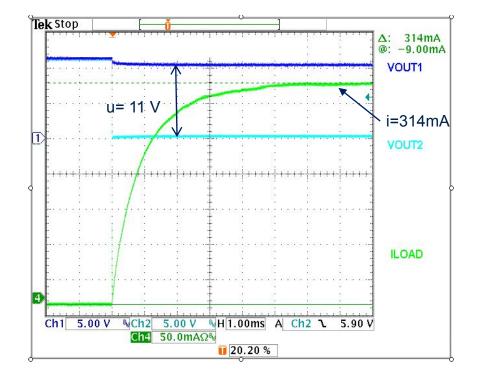
 $U = Kt * \omega + \mathbf{R} * i + L * d(i)/dt$

- The rotor is blocked
- When the steady state is reached :



• R = U / i





Smart Component Extraction (14) DC Motor Parameter extraction



$U = \mathbf{K}\mathbf{t} * \mathbf{\omega} + \mathbf{R} * \mathbf{i} + \mathbf{L} * \mathbf{d}(\mathbf{i})/\mathbf{d}\mathbf{t}$

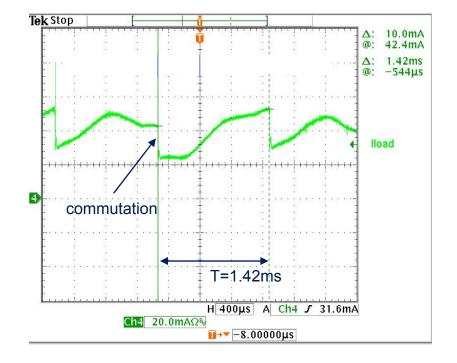
• The rotor rotates

- Kt extraction

- One rotation induces 4 current commutations in the motor
- The time between two commutations (1/4 rotation) is measured
- The angular velocity (ω_s) is deduced (1 rotation = 2π [rad])

 $\omega_s = 1106 \text{ rad/s}$

• Kt = U / ω_s



Kt = 9.95 mV/(rad/s)

Smart Component Extraction (15) DC Motor Parameter extraction

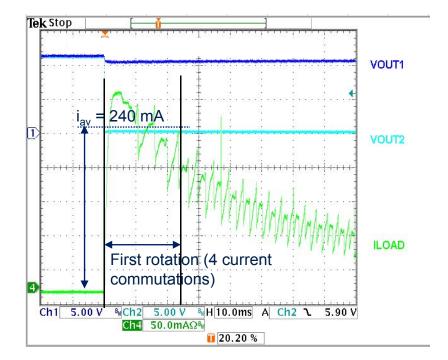


- J extraction :

 $T = -Kt * i + d * \omega + J * d(\omega)/dt$

- Motor in inrush without load
- The angular velocity reached after 25 ms (1 rotation) is read out
- The angular acceleration $(d(\omega)/dt)$ is then approximated
- The average current during the first rotation (iav) is read out
- T is the Torque delivered by the motor (= 0.0 without load)

• 0.0 = - Kt *
$$i_{av}$$
 + d * ω + J * d(ω)/dt
=0



J = 1.52e-7 Kgm²

Smart Component Extraction (16) DC Motor Parameter extraction

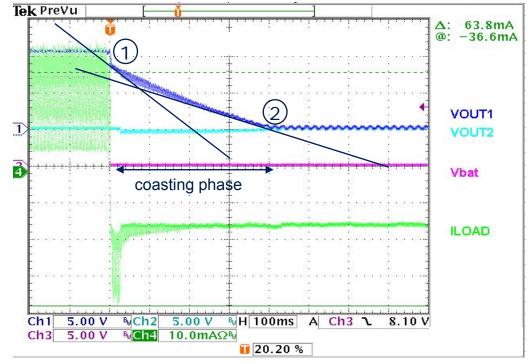


- D and Mr extraction :
- (Mr : constant friction)
 - The rotor is disconnected from the battery (i = 0.0 A), no load
 - The slopes are measured at the beginning (1) and at the end (2) of the coasting phase to get the angular acceleration ($\Delta \omega / \Delta t$))
 - The equation is evaluated at the beginning and at the end of the coasting phase to isolate D and Mr (with i = 0.0, T = 0.0)

(1) J * d(
$$\omega$$
)/dt = - Mr – d * ω_s

(2)
$$J * d(\omega)/dt = - Mr - d * \omega$$

T = - Kt * i + **d** * ω + J * d(ω)/dt + **Mr**



Mr = 3.73e-4 Nm

D = 1.69e-7 Nm/(rad/s)

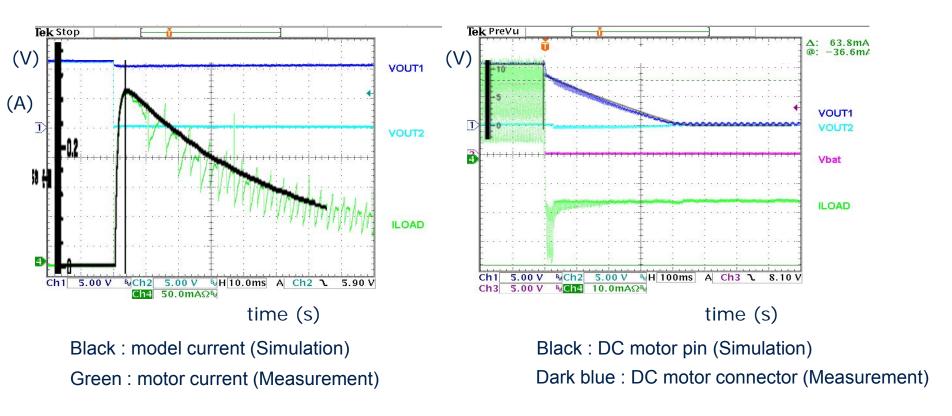
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Comparing Component measurements with simulation results



Motor in inrush

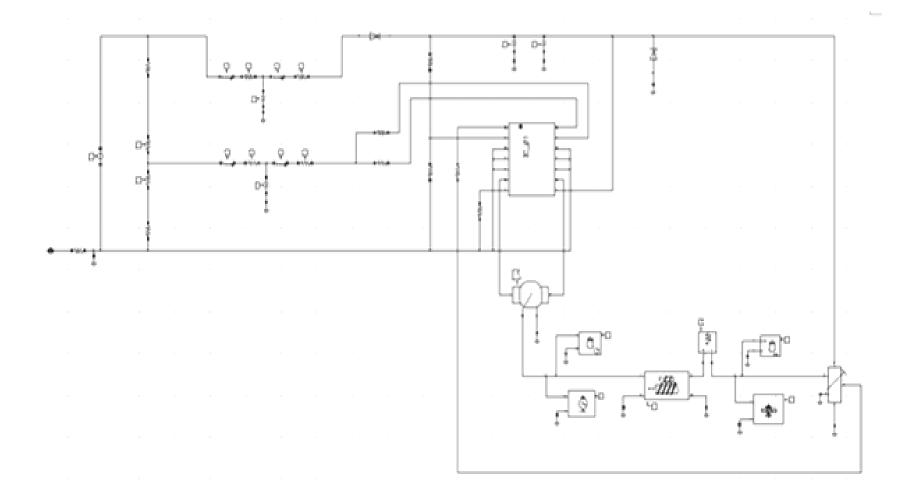
Coasting phase



Application Verification (simulation)



The Test Bench is the Application Model defined earlier



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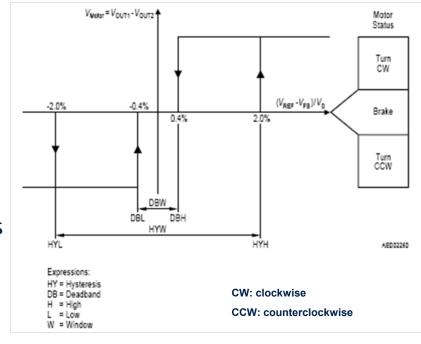
Application Verification (2) Tracking simulation

The typical servo behavior is investigated:

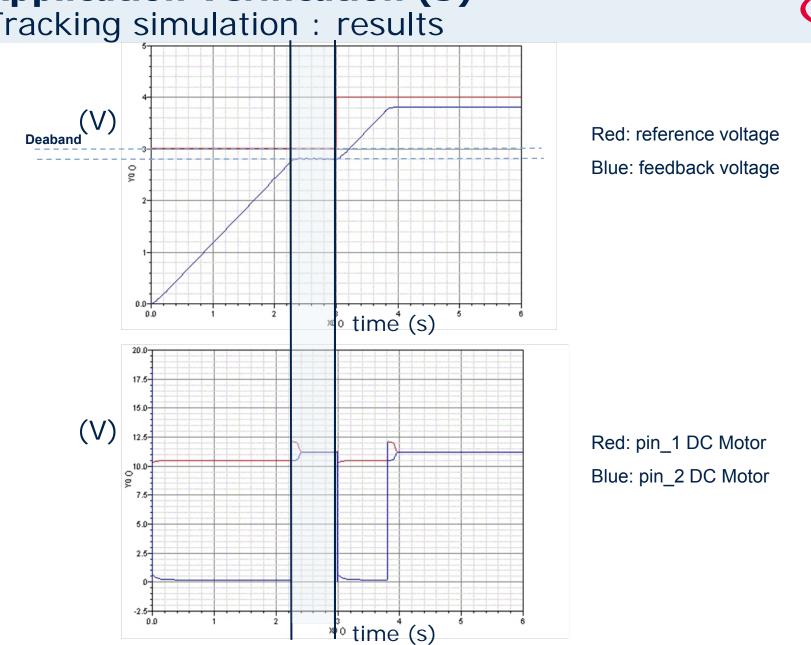
i.e. a reference is settled (input) and the feedback is observed (output)

Application typical behavior:

- To prevent oscillations, a degree of hysteresis is introduced between the reference and feedback signals
- To avoid high mechanical stress, the braking is carried gently over a period of time. This region between braking and stopping is referred to as deadband









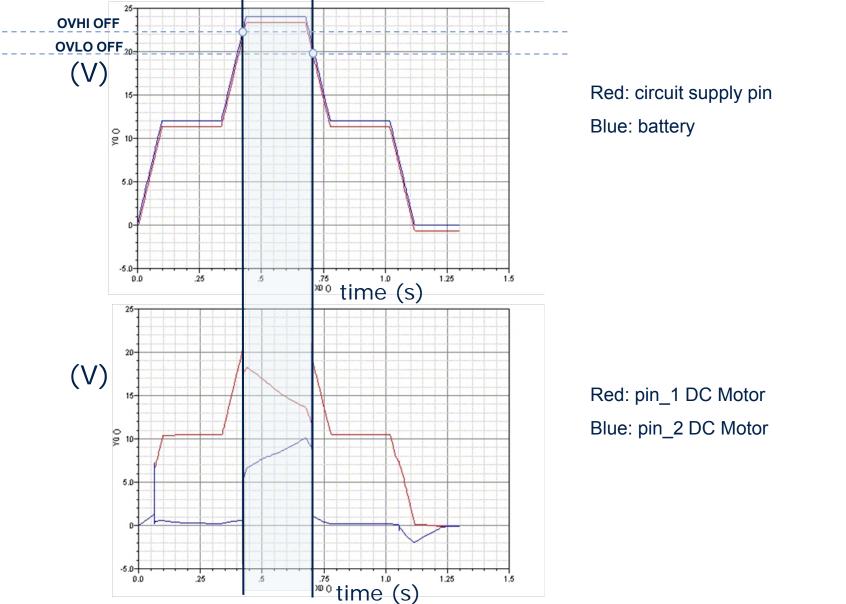
Application Verification (4) Overvoltage simulation



The Overvoltage Protection is investigated

- The Overvoltage Protection is implemented as follows:
 - The control circuit switches OFF the output stages to "High Impedance" if the supply voltage of the circuit reaches the overvoltage threshold OVHI OFF
 - The device switches on again when the supply voltage decreases to the OVLO OFF threshold, which is lower than the previous threshold (hysteresis)

Application Verification (5) Overvoltage simulation : results





CONCLUSION



Smart method to extract properties has been shown

Verification feasability has been illustrated

Open wide range of simulative activities

- Exhaustive Verification
- Robustness Investigation
- Worst Case
- Parametrization
- Effective sizing

□ ...



Thank you for your attention,

Questions?

Application Verification (4) Tracking simulation : results



