



System Level Modeling of Smart Power Switches using SystemC-AMS for Digital Protection Concept Verification

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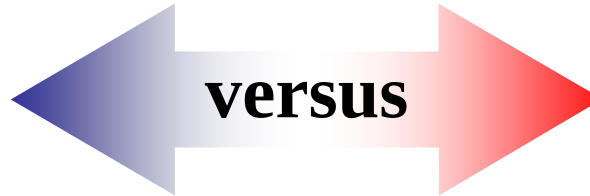
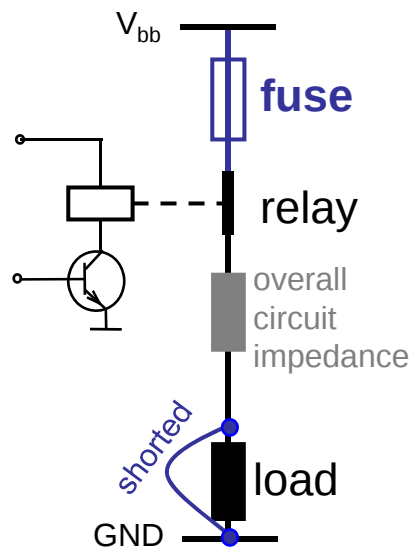


- Automotive & Smart Power devices
- Stress caused by inappropriate protection strategies
- System level model for a short circuit scenario
 - electro-(non-linear) thermal MOSFET model
 - controller model
- Simulation results and verification on HIL testbench using a test chip
- Conclusion

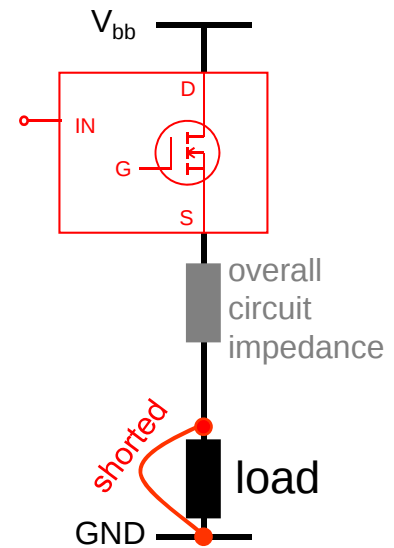
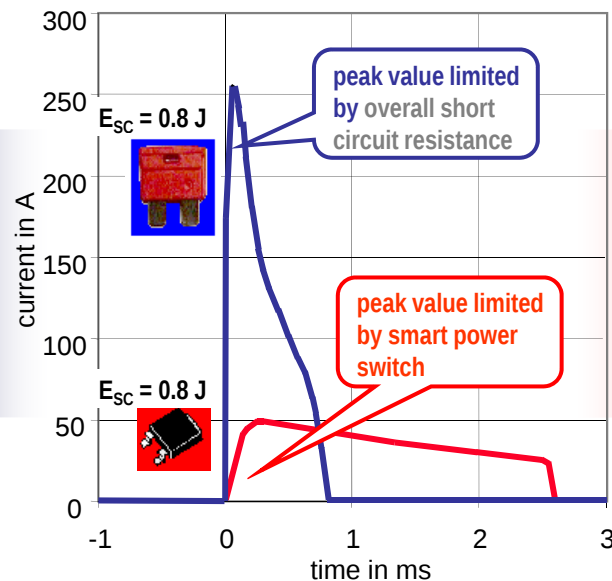
Smart Power switch application



Mechanical power switch application



Electronic Smart Power switch application



- Low cost & complexity
- Separate fuse required
- High peak current

- Integrated protection function
- Overcurrent limited
- Fault diagnosis available

Smart Power stage protection

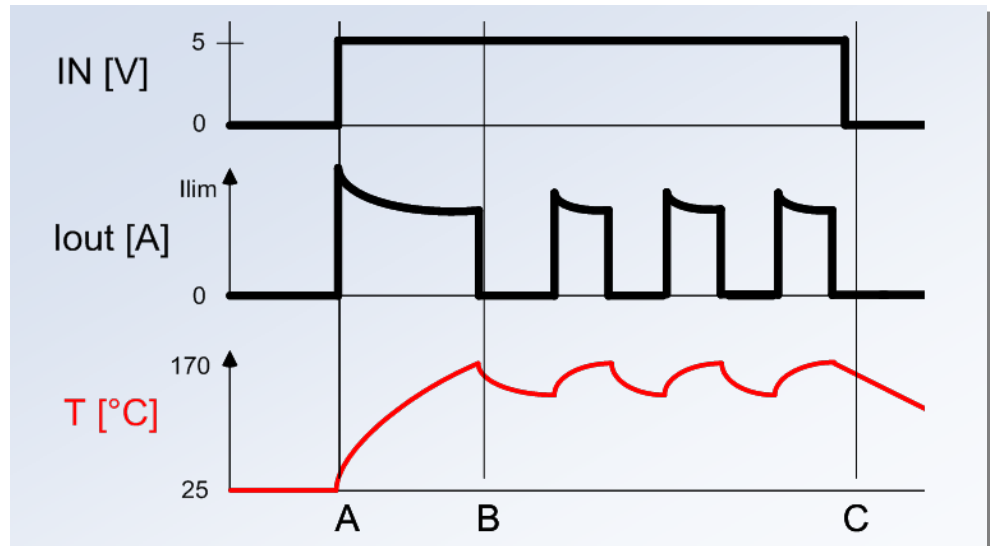
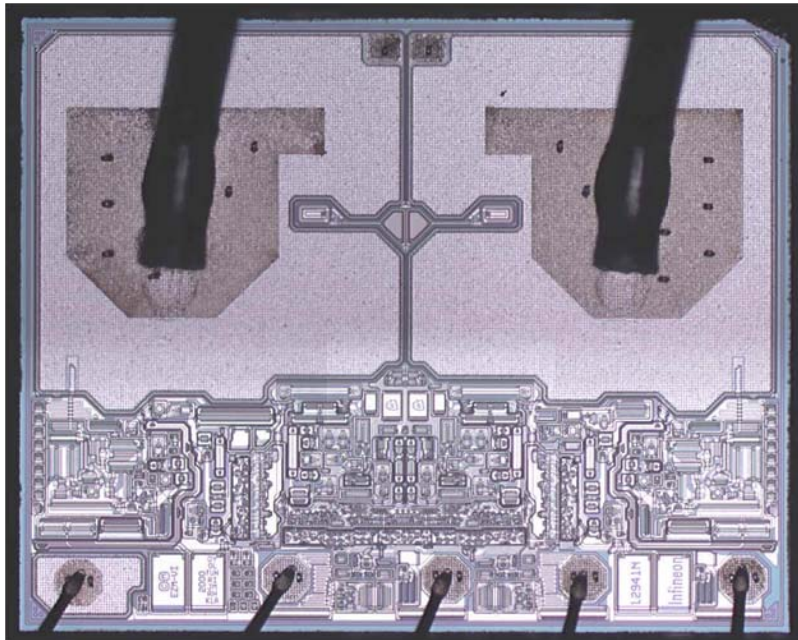
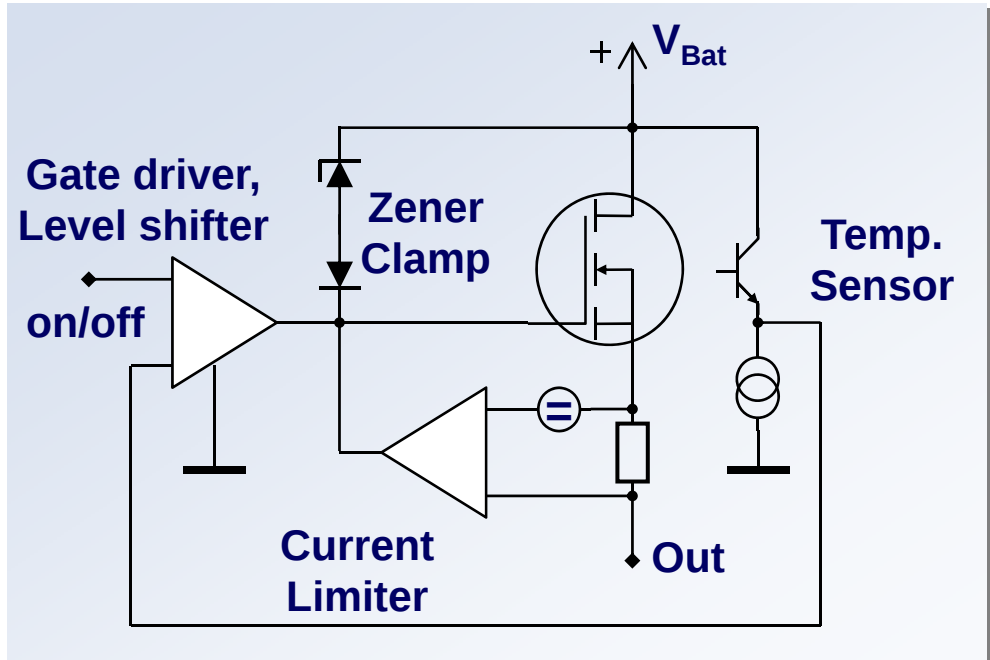


Protection mechanisms:

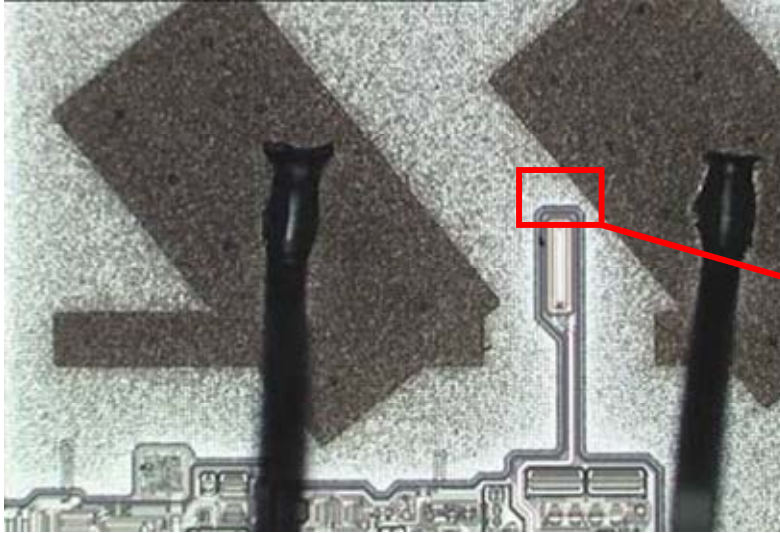
Current limitation $10 \times I_{Load}$

Thermal shutdown 170°C

Voltage clamping 50 V

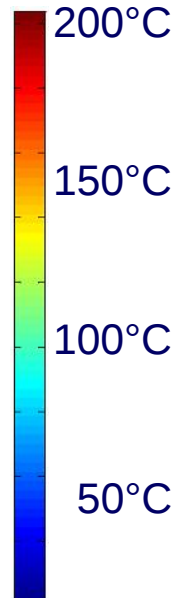
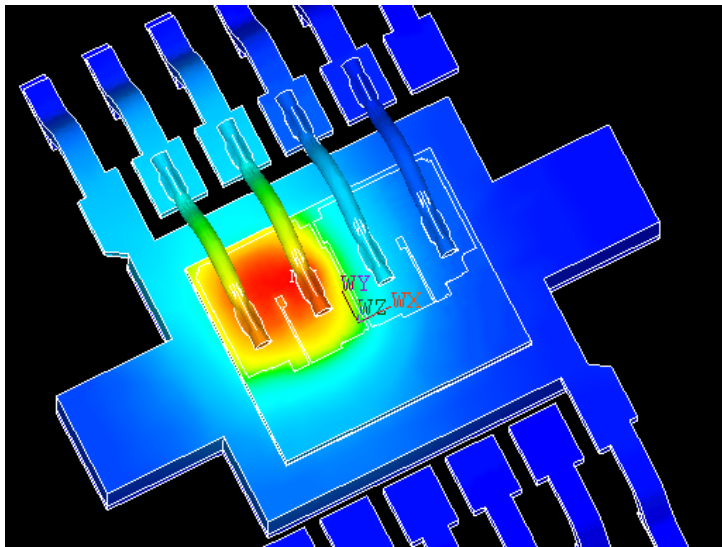
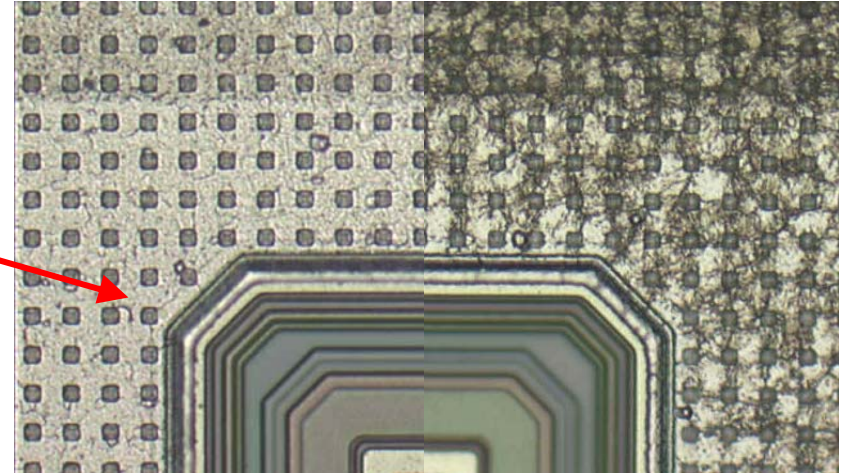


Protection strategy influences reliability



ORIGINAL
(new device)

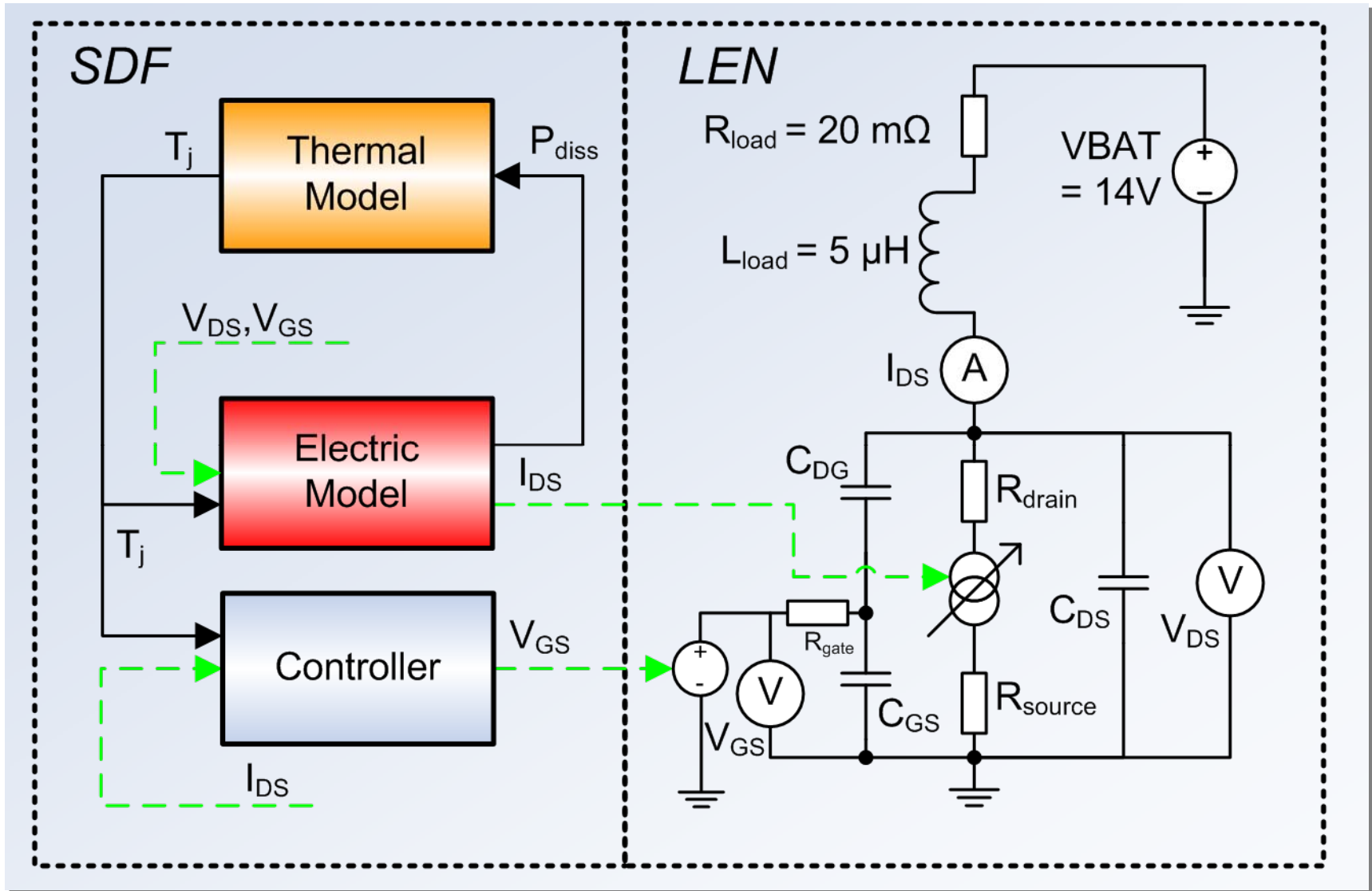
DEGRADED
(after 10k cycles)



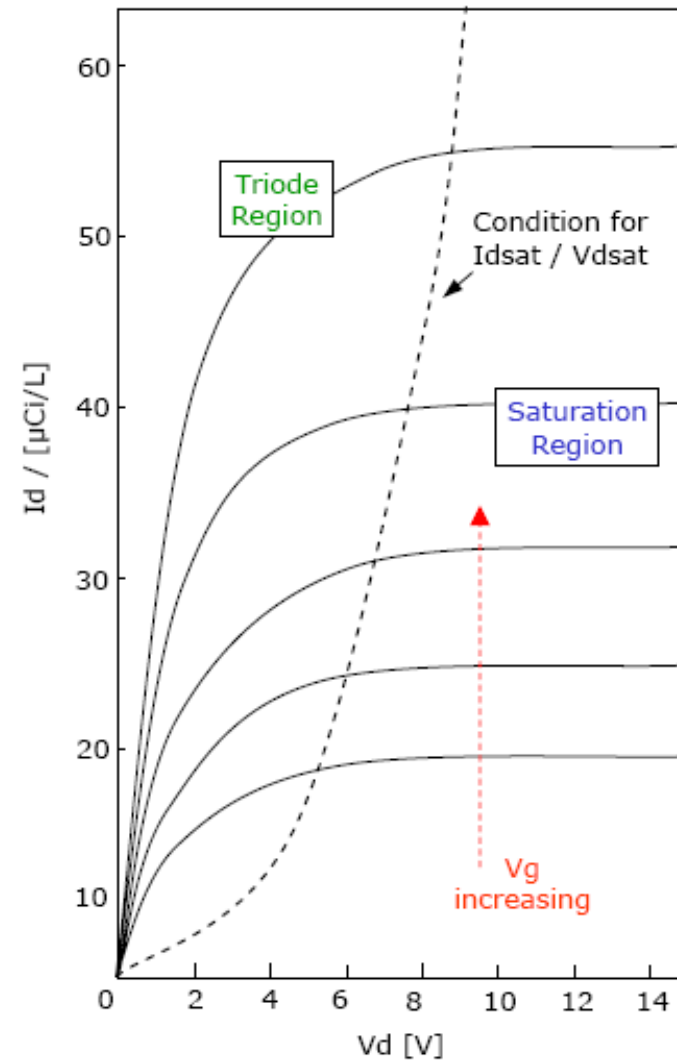
Design affects
RELIABILITY!

- Provide system level models of a SPS
 - Electro thermal model for the power stage
 - Description of gate driving unit (protection concept)
 - Load model – worst case scenario >>shorted load<<
 - Be ready to model more DIGITAL functionality (PWM ...)
- Verify the models on a HIL testbench

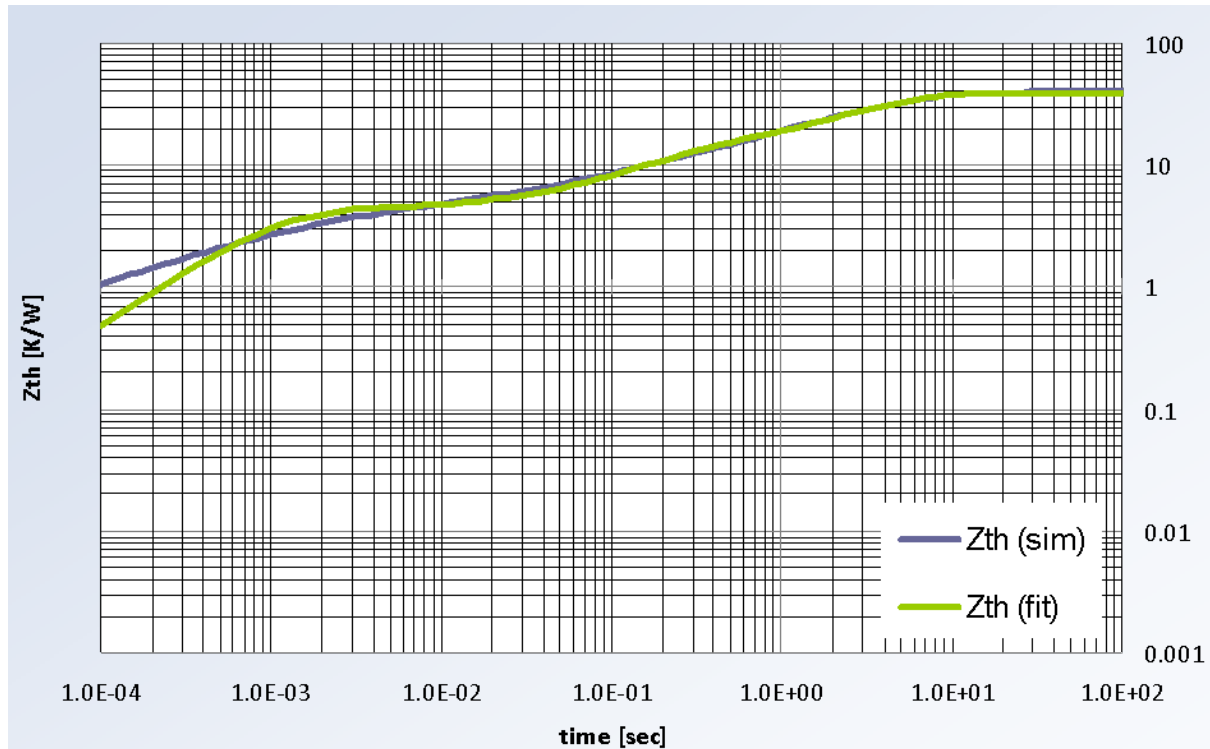
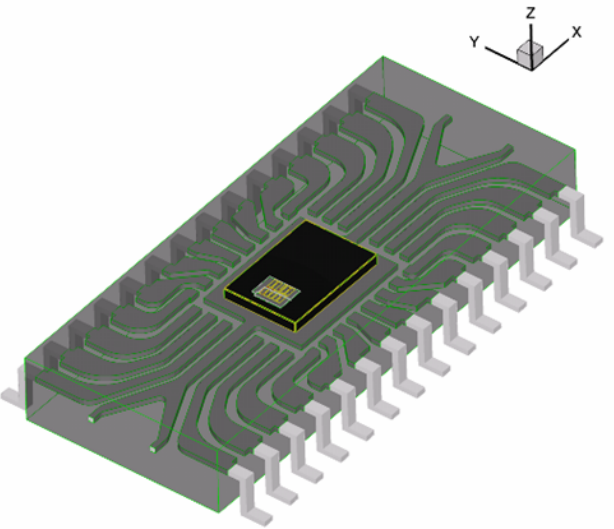
System level model for short circuit scenario



- Grove-Frohmman channel equation including thermal effects
- Meyer-Cap model
- Fitted for power MOSFET based on measurements and technology parameters

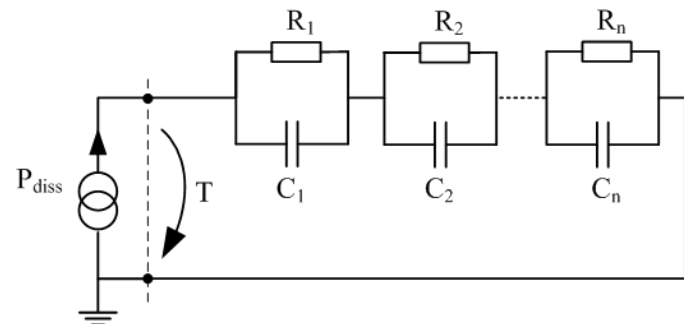


Thermal MOSFET model

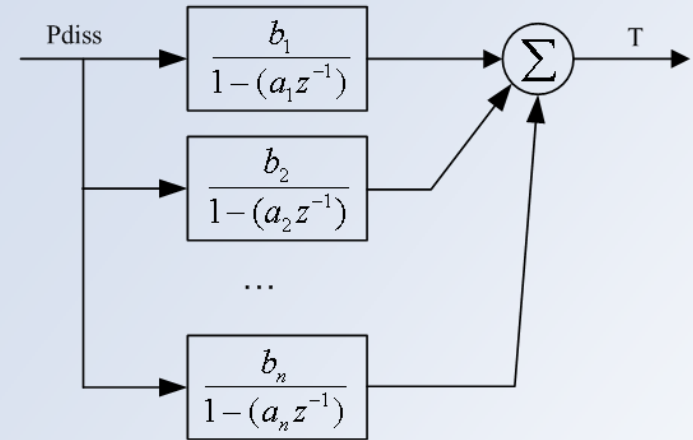
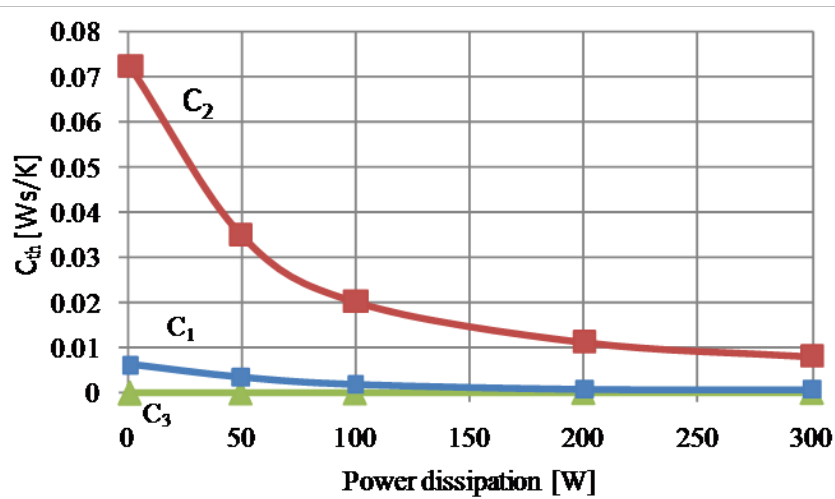
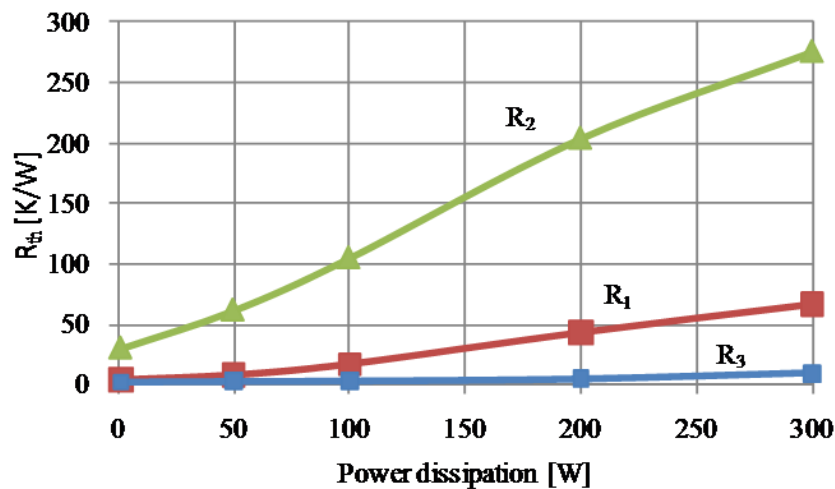


$$Z_{th}(t) = \sum_{i=1}^n R_i \left(1 - e^{-\frac{t}{R_i C_i}} \right)$$

- Obtain Z_{th} curve using FEM simulations
- Fit R_i/C_i with thermal step response of a Foster network in time domain



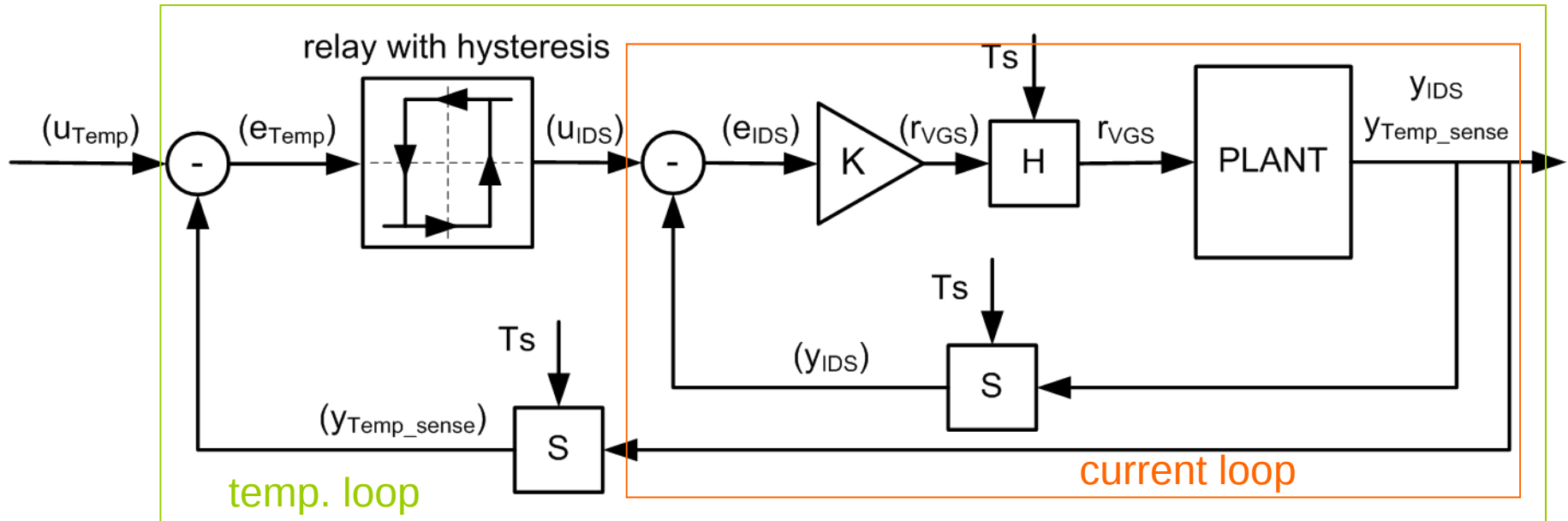
Nonlinear thermal MOSFET model



$$a_n = Ts \cdot \frac{f_{Rn}(P)}{1 + \frac{f_{Rn}(P) \cdot f_{Cn}(P)}{Ts}}$$

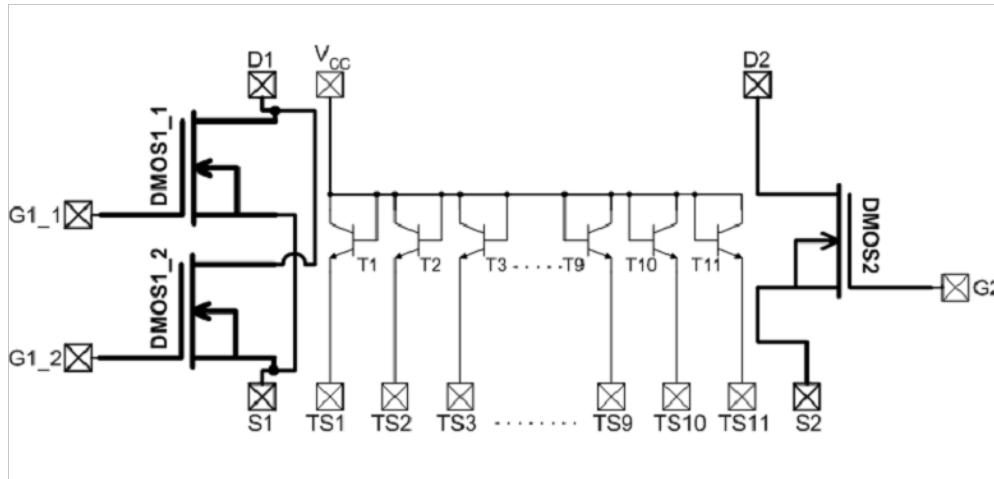
$$b_n = \frac{f_{Rn}(P) \cdot f_{Cn}(P)}{Ts + f_{Rn}(P) \cdot f_{Cn}(P)}$$

Controller Model

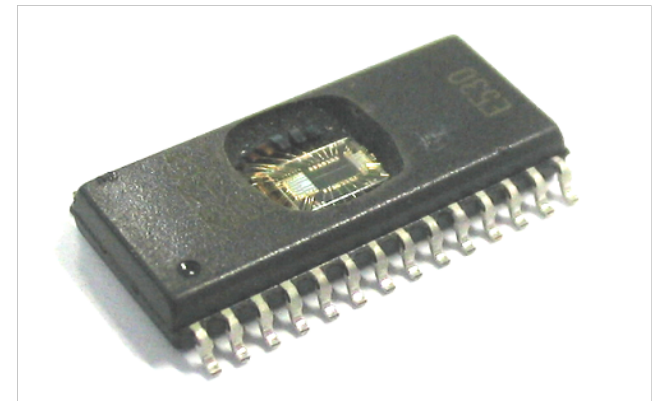
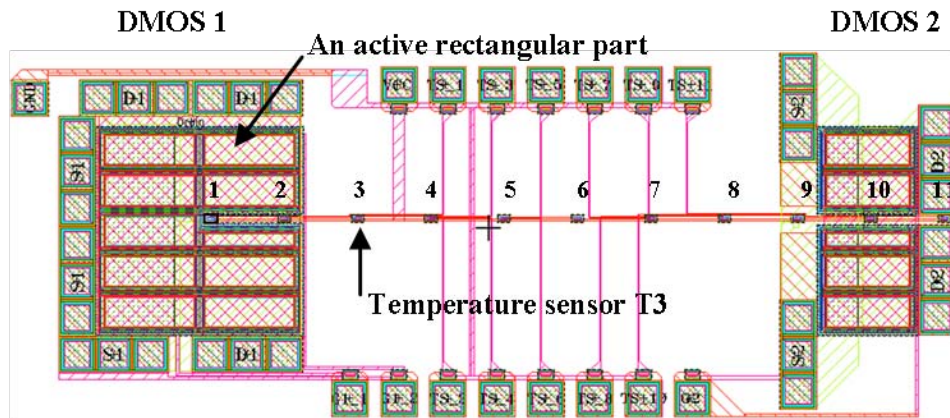


- Over temperature protection – thermal relay with hysteresis
- P-controller for current regulation

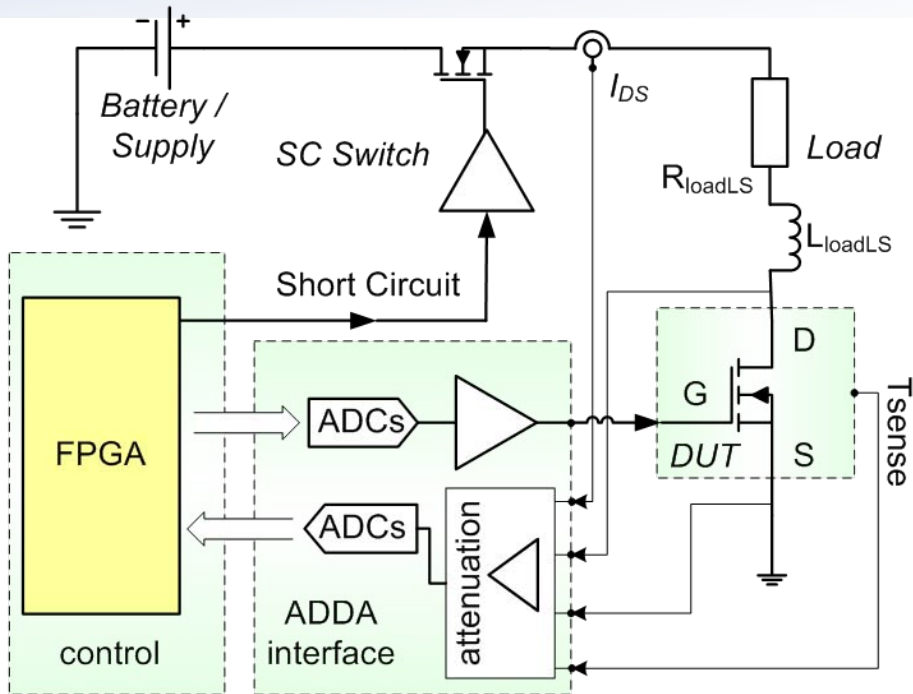
Model Verification - the test chip



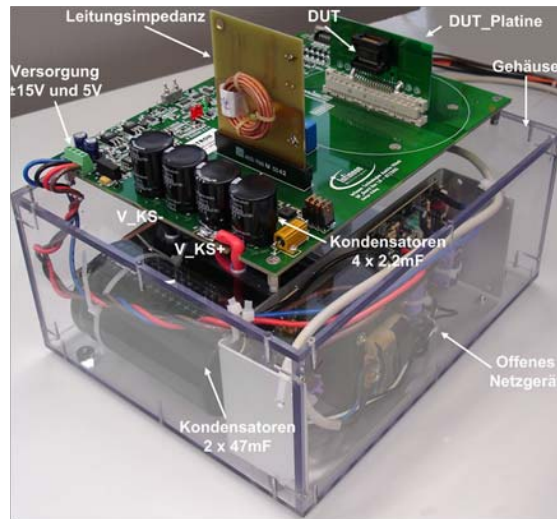
- 2 power MOSFETs
- 11 temperature sensors
- BCD technology
- assembled in P-DSO-28 plastic package



HIL test bench

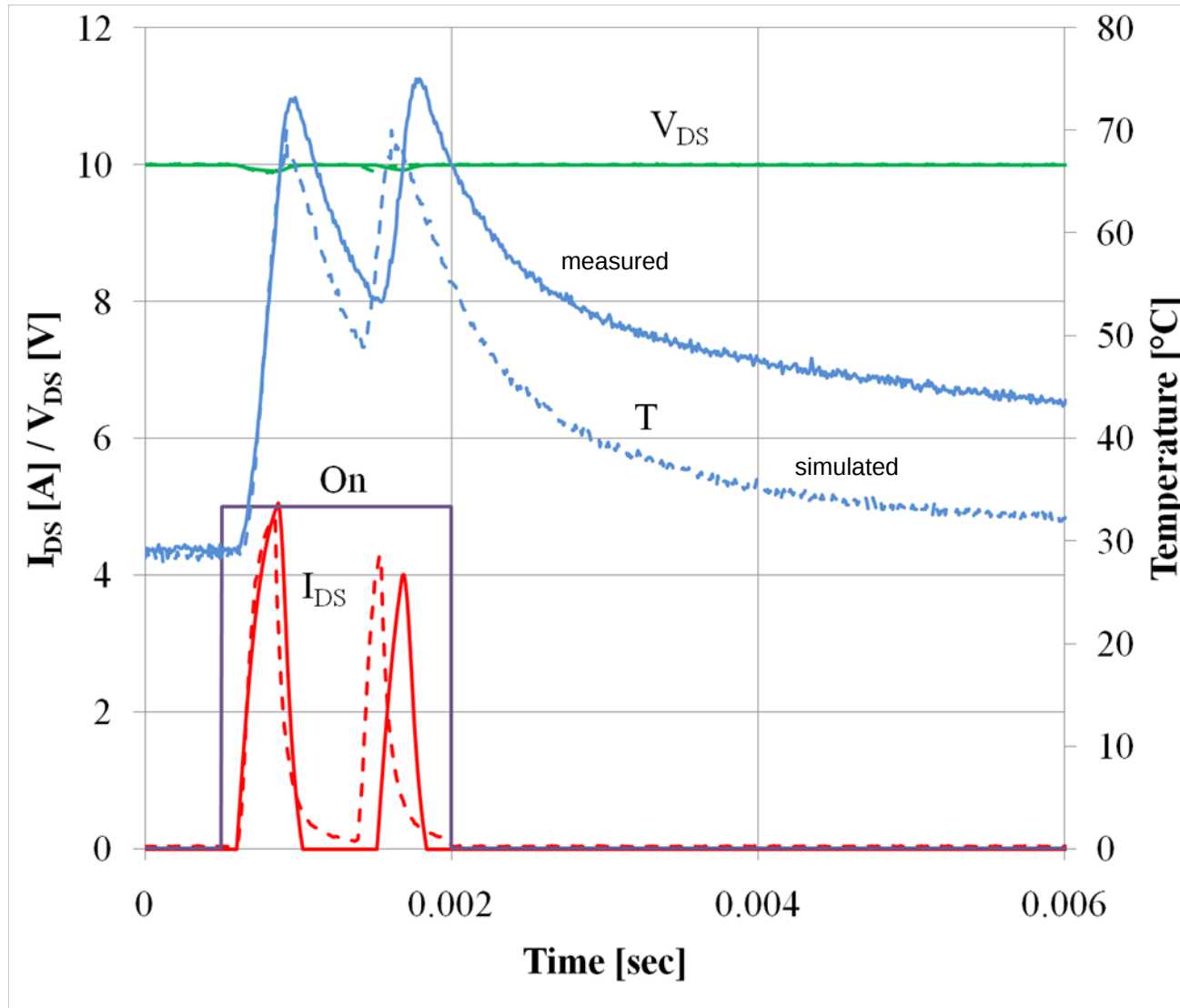


- switch up to 100 A
- over temperature and over current shutdown
- battery/supply up to 60 V
- R_{load}/L_{load} configurable
- FPGA for control and data acquisition
 - 40 MHz clock
 - 8 x AI@200 kS
 - 8 x AO@1 MS



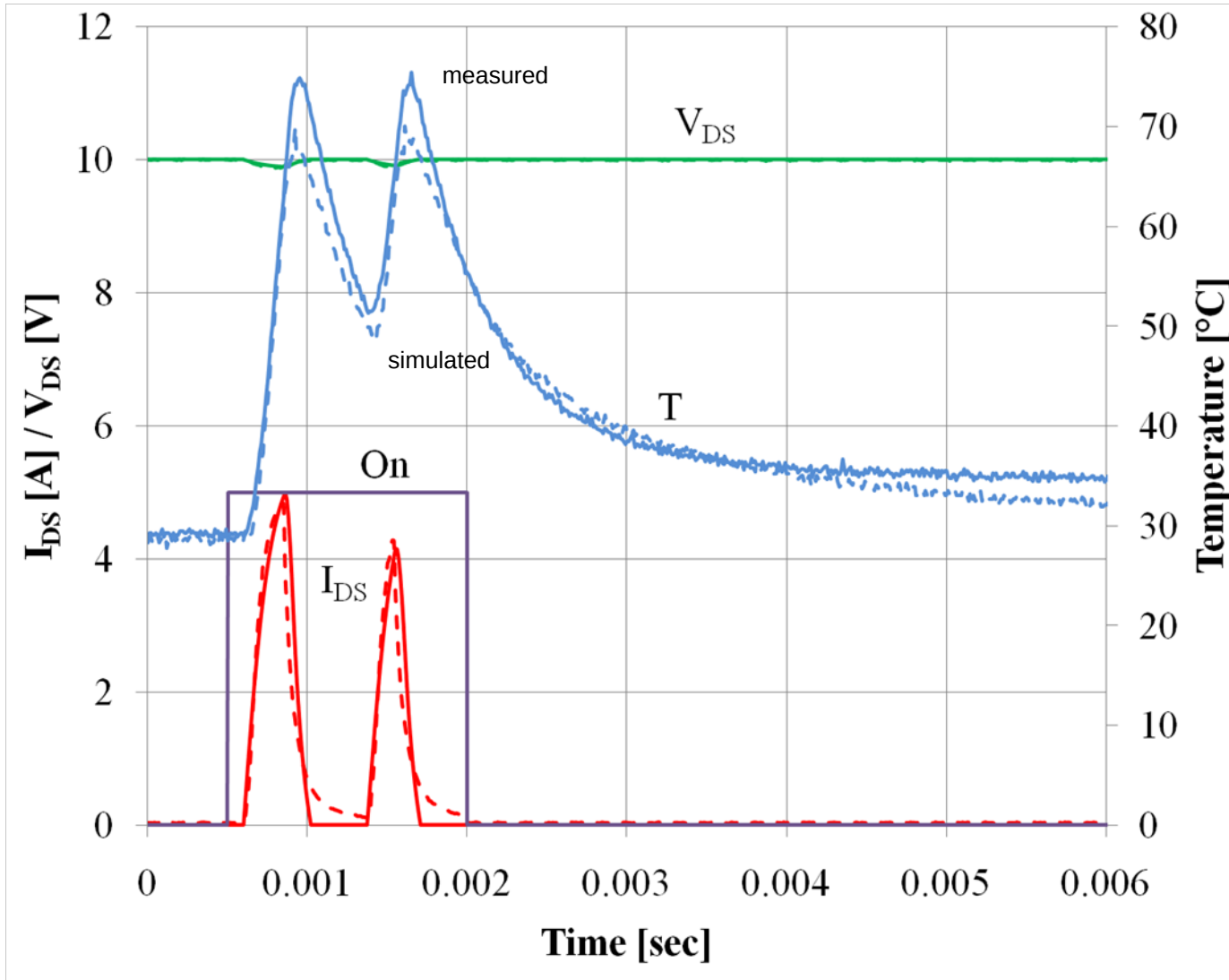
[Master thesis Robert Illing]

Measurement and Simulation Result (1)



- Linear temperature model leads to relatively large deviations

Measurement and Simulation Result (2)



➤ Using the non-linear temperature model results in better accuracy!

- An electro-thermal SystemC-AMS MOSFET model was developed
- Non-linear thermal Foster network was introduced
- SystemC-AMS testbench presented; power MOSFET, load (short circuit) and protection concept
- Successful verification using a HIL testbench was presented



**Thank You
for Your Attention!**

